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PART I

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**CHARACTERIZATION OF VERY PAUCI-DISPERSE
SYSTEMS WITH STRONG INTERACTION BY
EQUILIBRIUM SEDIMENTATION**

**PART I. DETERMINATION OF MOLECULAR WEIGHTS AND
PARTIAL EVALUATION OF INTERACTION MATRIX**

MATATIAHU GEHATIA

DONALD R. WIFF

TECHNICAL REPORT AFML-TR-69-235, PART I

JANUARY 1970

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PART I

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FOREWORD

This report was prepared by the Polymer Branch of the Nonmetallic Materials Division. The work was initiated under Project 7342, "Fundamental Research on Macromolecular Materials and Lubrication Phenomena," Task No. 734203, "Fundamental Principles Determining the Behavior of Macromolecules." The work was administered under the direction of the Air Force Materials Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio, with Dr. M. T. Gehatia acting as project scientist.

The report covers research conducted from January 1968 to April 1969. The manuscript was released by the author in May 1969 for publication as a technical report.

This technical report has been reviewed and is approved.

William E. Gibbs

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ABSTRACT

As part of a series of investigations of the fundamental properties of certain aromatic-heterocyclic polymers, a study has been done on the equilibrium sedimentation of samples of poly (2,2'-m-phenylene-5,5'-bibenzimidazole) in dimethylacetamide. Although these samples were obtained by fractional precipitation techniques from a whole polymer, it was found that their behavior was best described by assuming some samples to be composed of at least two major sub-fractions. In addition, this analysis required that each sub-fraction have a relatively strong interaction with itself and other sub-fractions. Because each sample consisted of a small number of major fractions a method was developed based upon considerations from pauci-disperse systems to characterize molecular weights and polymer-polymer interaction terms. This report details the development of this method. The concentration of these samples is represented by:

$$c \approx \sum_{n=1}^N g_n \exp \left[h_n \omega^2 x - R_{nk} c + (R_{nk} - R_{nn}) c_n \right],$$

where c is concentration; x = square of the distance from the center of rotation; h_n a constant proportional to molecular weight of fraction n ; R_{nk} , R_{nn} are interaction coefficients and ω is the angular velocity.

The distribution of this Abstract is unlimited.

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LIST OF SYMBOLS

r = the distance from the center of rotation
 r_m = the distance from the center of rotation to the meniscus
 r_b = the distance from the center of rotation to the bottom of the cell
 x = r^2
 m = r_m^2
 b = r_b^2
 r_o = the distance from the center of rotation to the initial boundary in a velocity experiment
 s = sedimentation constant
 D = diffusion constant
 ω = angular velocity
 β = $h\omega^2$
 t = time
 T = absolute temperature in °K
 R = universal gas constant, or interaction parameter in general
 ρ = density of solution
 ρ_o = density of solvent
 V = partial specific volume of polymer in solution
 c = concentration in g of polymer per g of solution
 c^* = initial concentration
 H = $2RT/(1-V\rho)$
 M = molecular weight
 h = M/H
 g = a constant defined for θ -temperature where, $g = c e^{-h\omega^2 x}$

LIST OF SYMBOLS (CONT)

 c_n c^*_n M_n h_n g_n

$\left. \begin{array}{l} c_n \\ c^*_n \\ M_n \\ h_n \\ g_n \end{array} \right\}$ the above defined quantities corresponding to fraction n,
 R_{nk} = interaction parameter appearing in an expression for c_n , and
caused by c_k

SECTION I

INTRODUCTION

Aromatic-heterocyclic polymers are a class of interesting materials that are currently being developed due to their resistance to high temperature. Relatively little has been done toward determining many of the fundamental parameters that govern the physical behavior of these chains. This report covers one phase of an investigation of the dilute solution properties of one of the earlier, high molecular weight aromatic-heterocycles, poly (2,2'-m-phenylene-5,5'-bibenzimidazole) (PBI), dissolved in a good solvent dimethylacetamide (DMAC). Specifically this report concerns equilibrium sedimentation measurements on samples of this polymer in an effort to define molecular weight, and polymer-polymer interaction parameters.

Preliminary measurements on these samples suggested that each sample consists of a relatively small number of rather discrete molecular weight ranges. In addition, it was suspected that relatively strong interactions could exist between various species. Therefore, early consideration was given to describing this situation by applying a method developed from study of pauci-disperse systems.

This is discussed in the next section.

SECTION II

THEORY

A MONODISPERSE SYSTEM WITH INTERACTION

Consider a monodisperse polymer with significant concentration dependence. If higher than first order terms can be neglected, the concentration achieved in equilibrium-sedimentation can be expressed by the following equation:

$$c = g e^{\hbar \omega^2 c - R c} \quad (1)$$

The relationship expressed by Equation 1 and especially the interaction parameter R were discussed by Fujita (Reference 1), Casassa (Reference 2), Gehatia and Wiff (Reference 3), and others.

By differentiating Equation 1 with respect to x one obtains:

$$\frac{dc}{dx} = \left(\hbar \omega^2 - R \frac{dc}{dx} \right) c \quad (2)$$

which leads to the following working formulas:

$$c^{-1} \frac{dc}{dx} = \hbar \omega^2 - R \frac{dc}{dx} \quad (3)$$

$$c^{-1} = \hbar \omega^2 \left(\frac{dc}{dx} \right)^{-1} - R \quad (4)$$

A plot of $c^{-1} \frac{dc}{dx}$ vs. $\frac{dc}{dx}$, according to Equation 3, should give a straight line with a slope equal to $(-R)$. Similarly, according to Equation 4, a plot of c^{-1} vs. $\left(\frac{dc}{dx} \right)^{-1}$ gives a slope equal to $\hbar \omega^2$, which is a quantity proportional to the molecular weight (References 3 and 4).

By knowing $\hbar \omega^2$ and R one can evaluate the constant g from Equation 1 and thereby fully characterize the system under consideration.

SYSTEM OF TWO DISTINCT INTERACTING FRACTIONS

Consider a solution of polymer comprised of two interacting fractions (1 and 2). The concentration can be expressed as:

$$c = c_1 + c_2 \quad (5)$$

where:

$$c_1 = g_1 e^{h_1 \omega^2 x} - R_{1,1} c_1 - R_{1,2} c_2 \quad (6)$$

and:

$$c_2 = g_2 e^{h_2 \omega^2 x} - R_{2,1} c_1 - R_{2,2} c_2 \quad (7)$$

It has been assumed that in a certain region ($m \leq x \leq x^*$) the fraction 1 prevails, e.g., that $c_1 \approx c$ and $c_2 \ll c_1$. Since $c_1 = c - c_2$ the exponent in Equation 6 can be modified:

$$-R_{1,1} c_1 - R_{1,2} c_2 = -R_{1,1} c - (R_{1,2} - R_{1,1}) c_2 \quad (8)$$

and Equation 5 can be approximated by the formula:

$$c \approx g_1 e^{h_1 \omega^2 x} - R_{1,1} c \left[1 - (R_{1,2} - R_{1,1}) c_2 \right] + c_2 \quad (9)$$

Denote:

$$g_1 e^{h_1 \omega^2 x} - R_{1,1} c = G_1 \quad (10)$$

and:

$$R_{1,2} - R_{1,1} = K_m \quad (11)$$

Equation 9 will now lead to the following expression for c_2 :

$$\frac{c - G_1}{1 - K_m G_1} \approx c_2 \quad (12)$$

The approximation is justified if the quantity $K_m c_2 \ll 1$, e.g., if, for a certain $x > x^*$, c_2 is not negligible in comparison to be c , but is still small enough to make the following transformation valid:

$$e^{-K_m c_2} \approx 1 - K_m c_2 \quad (13)$$

For a known value of K_m one can evaluate the c_2 curve in a region in which $K_m c_2 \ll 1$. According to Fujita (Reference 1),

$$R_{1,2} = M_1 f_{1,2} \quad (14)$$

and:

$$R_{2,1} = M_2 f_{2,1} \quad (15)$$

where f_{12} and f_{21} are the cross coefficients of interaction and:

$$f_{1,2} = f_{2,1} \quad (16)$$

Using this assumption of a symmetric interaction one obtains:

$$R_{2,1} = R_{1,2} \left(\frac{M_2}{M_1} \right) = R_{1,2} \left(\frac{h_2 \omega^2}{h_1 \omega^2} \right) \quad (17)$$

By inserting this expression for $R_{2,1}$ into Equation 7 one obtains the following formula:

$$\ln c_2 = \ln g_2 - \frac{h_2 \omega^2}{h_1 \omega^2} R_{1,2} c + \left[\frac{h_2 \omega^2}{h_1 \omega^2} R_{1,2} - R_{2,2} \right] c_2 \quad (18)$$

Equation 18 is an expression for c_2 with three unknown parameters; $\ln g_2$, $(h_1 \omega^2/h_2 \omega^2) R_{1,2} = a$, and $\left[(h_2 \omega^2/h_1 \omega^2) R_{1,2} - R_{2,2} \right] = b$

For a large number of c values one can determine the parameters in Equation 18 as well as the total error of the system. In this calculation a measure of the error was taken as:

$$\Delta_m^2 = \sum_i \delta_{m,i}^2 \quad , \quad (19)$$

where:

$$\delta_{m,i} = \ln (c_2)_{m,i} - \ln (g_2)_m + a_m(c)_i + b_m(c_2)_{m,i} \quad (20)$$

One must remember that such a treatment was originally suggested for the case when K_m is a known quantity. In a real case such a value is not known, a priori. However, the following procedure can be applied. A set of values can be assumed for K_m and accordingly Δ_m^2 can be evaluated. The "best fit," e.g.,

the minimum of a plot Δ_m^2 vs. K_m , gives an acceptable value for K_m . In such a case the values of K_m as well as other parameters, are determined. These parameters finally lead to evaluation of the following constants: M_1 , M_2 , g_1 , g_2 , $R_{1,1}$, $R_{1,2}$, $R_{2,1}$, and $R_{2,2}$, which fully describe the system comprised of two interacting fractions (Figures 16 and 17).

The search for appropriate K_m values can be accomplished by use of a high speed computer. In case of a few fractions one can find more than one distinct K_m value, i.e., $\{K_{m,n}\}$; with the corresponding set M_n , g_n , R_{1n} , R_{ni} , and R_{nn} . If there are too many fractions in the system $K_{m,n}$ values cannot be distinguished by searching, and "noise" is created.

In case of two fractions, and if all parameters of the transcendental equation, Equation 7, are known, c_2 can be precisely evaluated for all values of x without need of an approximation.

SECTION III

EXPERIMENTAL

Bulk PBI was dissolved in DMAC and fractionated with hexane. The fractions were purified in the following manner. Each sample was redissolved in DMAC, precipitated and washed with methyl ethyl ketone (MEK), filtered and washed again with MEK. The process of washing was continued; however, MEK was replaced by mixtures of MEK-MEOH with successively decreasing amounts of MEK. The polymer was further washed with pure methanol and replaced by mixtures of MEOH-ether with successively decreasing amounts of MEOH. Finally, the remaining polymer was washed with ether and dried under vacuum (this method of purification and fractionation was suggested by T. E. Helminiak).

A set of sedimentation equilibrium experiments was carried out with four samples of PBI in DMAC at 40°C. An aluminum, 12mm, 4°, single sector cell containing the solution and another similar cell with DMAC were inserted into a J-rotor. The resulting Schlieren curves appeared, therefore, with a base line in addition to the sedimentation curve (Figures 2-8).

Each sample was measured at different rotor speeds. It required about 14-17 days to achieve the first equilibrium. If the speed was decreased the next equilibrium could be achieved within 7-10 days. However, it took only a few days to achieve equilibrium when the speed was increased rather than decreased. This surprising behavior, which contradicts theoretical considerations and expectations, has not yet been explained. In several cases no equilibrium was achieved as the speed was lowered and the Schlieren curve dissipated.

The quantity $\frac{dc}{dn}$ has been determined from auxiliary velocity runs carried out with a synthetic boundary cell.

Finally the plates were enlarged and the coordinates $\frac{dn}{dr}$ and Δr were measured.

SECTION IV

COMPUTATION

The experimental data was analyzed by applying Equations 3 and 4. (Figures 2-16 and Tables I-XI). As one can readily see no linear plots have been obtained. Therefore, the samples under consideration are not homogenous. On the other hand, one can also observe that these plots clearly show a straight line in a zone close to the meniscus ($m \leq x \leq x^*$, where x^* is a special value different for each sample and speed). Only sample three led to a straight line over all values of x .

Such a peculiarity of the plot can be explained by assuming the existence of a distinct low molecular weight fraction. This, as well as other considerations, suggests that there exists a very pauci-disperse system, i.e., that each sample is comprised of a few fractions (as a matter of fact, 2, 3, or 4 fractions). In addition, the low molecular weight fraction is very distinct in a certain zone near the meniscus, $c_{\text{total}} \approx c_1$ and $c_{n \neq 1} \ll c_1$.

The results of applying a method based upon these considerations to the four samples is summarized in Table XII. An equilibrium sedimentation experiment was made at each speed indicated. The first fraction parameters (g_1 , M_1 , and $R_{1,1}$) were evaluated by the procedure outlined above. The other parameters (g_m , M_m , R_{mm} , and R_{1m}) were determined by finding minima as indicated in Figure 22. All minima corresponding to fractions within a sample are indicated in Table XII.

SECTION V

DISCUSSION OF RESULTS

The computation just described cannot be considered as completed. In the case of four fractions:

$$c_n = g_n \exp (h_n \omega^2 - R_{n1} c_1 - R_{n2} c_2 - R_{n3} c_3 - R_{n4} c_4) \quad (21)$$

each curve can be evaluated within a zone, where $K_m c_m \ll 1$, and the corresponding parameters can be determined within such a zone.

However, an assumption has been made, according to Fujita (Reference 1), that:

$$\frac{R_{nk}}{M_n} = \frac{R_{kn}}{M_k} \quad (22)$$

which is not readily apparent (Reference 2). Without using the relationship described in Equation 22, the cross-coefficients R_{kn} ($k \neq 1$) cannot be easily evaluated.

The parameters $h_1 \omega^2$ and $R_{1,1}$ were determined from the linear portion of original plots. However, such an evaluation may introduce a numerical error which exceeds the tolerances required by the $K_{m,n}$, $\Delta_{m,n}$ analysis. Therefore, a variance in the values of $h_1 \omega^2$ and $R_{1,1}$ has to be taken into account to better fit the system.

Finally, the analysis has been performed by comparing the lowest fraction of a given sample with the other fractions in the sample. The results of applying this analysis to four samples is given in Table XII. Samples 1, 2, and 4 show that they are composed of about four sub-fractions. These sub-fractions have molecular weights of approximately 1,500; 30,000; 60,000; and 120,000. One sample, namely number 3, appears to have a very narrow distribution. Its weight average molecular weight is about 4,500.

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It is also significant that the diagonal elements (R_{mm}) of the "interaction" matrix were all found to be negative. Only values for R_{1m} are given in Table XII, since no proper method was applied to determine the off-diagonal elements R_{nk} for $n \neq 1$.

It has been suggested that some of the molecular weights indicated (Table XII) by this experimental analysis are higher than would be expected from condensation polymerization. Therefore, further investigations must be initiated for better examination of the system. Also, additional work will be required to more fully evaluate the validity of this method and to make necessary modifications to include in the calculation of all R_{nk} parameters.

SECTION VI

COMPUTER PROGRAM

COMPUTER SYMBOL IDENTIFICATION

Following is a list of symbols used in the computer program. Where possible the symbols are identified with the previously derived theory. One must remember that the computer program was written only for the case of two major distinct molecular weight components.

REC \varnothing RD - Used as "flag" for subroutine calling order.

PNAME1 and PNAME2 - Identification of experiment.

NMAX - Number of data points read into machine.

CO - Initial concentration of experimental solution.

R1 - First radial value. The distance from the center of rotation in the meniscus.

DLR - Incremented value for radial distances. Radial distance to the bottom of cell is given by R1 + (NMAX-1)*DLR.

R(I) - Array of radial values

X(I) - Array R(I)**2

CR(I) - Array containing experimentally measured ordinates from Schlieren Curves. Once these are read they are multiplied by SCALE to obtain the true $\frac{dc}{dr}$ values.

CX(I) - Array $(\frac{1}{2r}) (\frac{dc}{dr})$

C(I) - Array of concentrations obtained from $\int_m^x \frac{dc}{dx} dx = c - c_m$. Then use is made of the equation $\int_m^b c dx = c^o(b-m)$ to calculate c_m , the concentration at the meniscus.

ZLC(I) - Array $\ln (C(I))$

CX \varnothing VX(I) - Array $(dc/dx)/C$

XCX(I) - Array $(dc/dx)^{-1}$

Part I

 $XC(I) - \text{Array } (C^{-1})$ $NMAX1 - \text{First point at which } c_2 \text{ is small but must be considered.}$ $NMAX2 - \text{Highest point at which } c_2 \text{ is small but not zero.}$ $DLK - R_{1,1} + R_{1,2}$ $DKMAX - \text{Maximum value of DLK.}$ $XDLK - \text{Increment value for DLK.}$ $G(I) - \text{Array } \{ g_1 e^{h_1 \omega^2 x} - R_{11} c \}$ $H10MSQ - h_1 \omega^2$ $R11 - R_{1,1}$ $G1 - g_1$ $Y(I,J) - \text{Array containing three consecutive sets of values (three successive DLK values) for } YN(I).$ $YN(I) - (C(I) - G(I))/(1 - DLK * G(I))$ $U(I) - \text{Array } (X - (R_{12}/h_1 \omega^2) * c)$ $TY(I,J) - \text{Array containing the values of NMAX1 and NMAX2 corresponding to the array } Y(I,J).$ $Z(I) - \text{Array } \ln C_2(I)$ $R22 - R_{2,2}$ $R12 - R_{1,2} = DLK - R_{1,1}$ $G2 - g_2$ $H20MSQ - h_2 \omega^2$ $XLNG2 - \ln (g_2)$ $XN - \text{Number of data points sampled (NMAX2-NMAX1 + 1)}$

$$\begin{aligned}
 \text{DELTA} = & \frac{1}{XN} \sum_{i=NMAX1}^{NMAX2} \left\{ \ln c_2(x_i) - \left[\ln g_2 + h_2 \omega^2(x_i) - \frac{R_{1,2}}{h_1 \omega^2} c(x_i) \right. \right. \\
 & \left. \left. + \frac{R_{1,2}}{h_1 \omega^2} - R_{2,2} c_2(x_i) \right] \right\}^2
 \end{aligned}$$

The flow of computer data is shown in Figure 1.

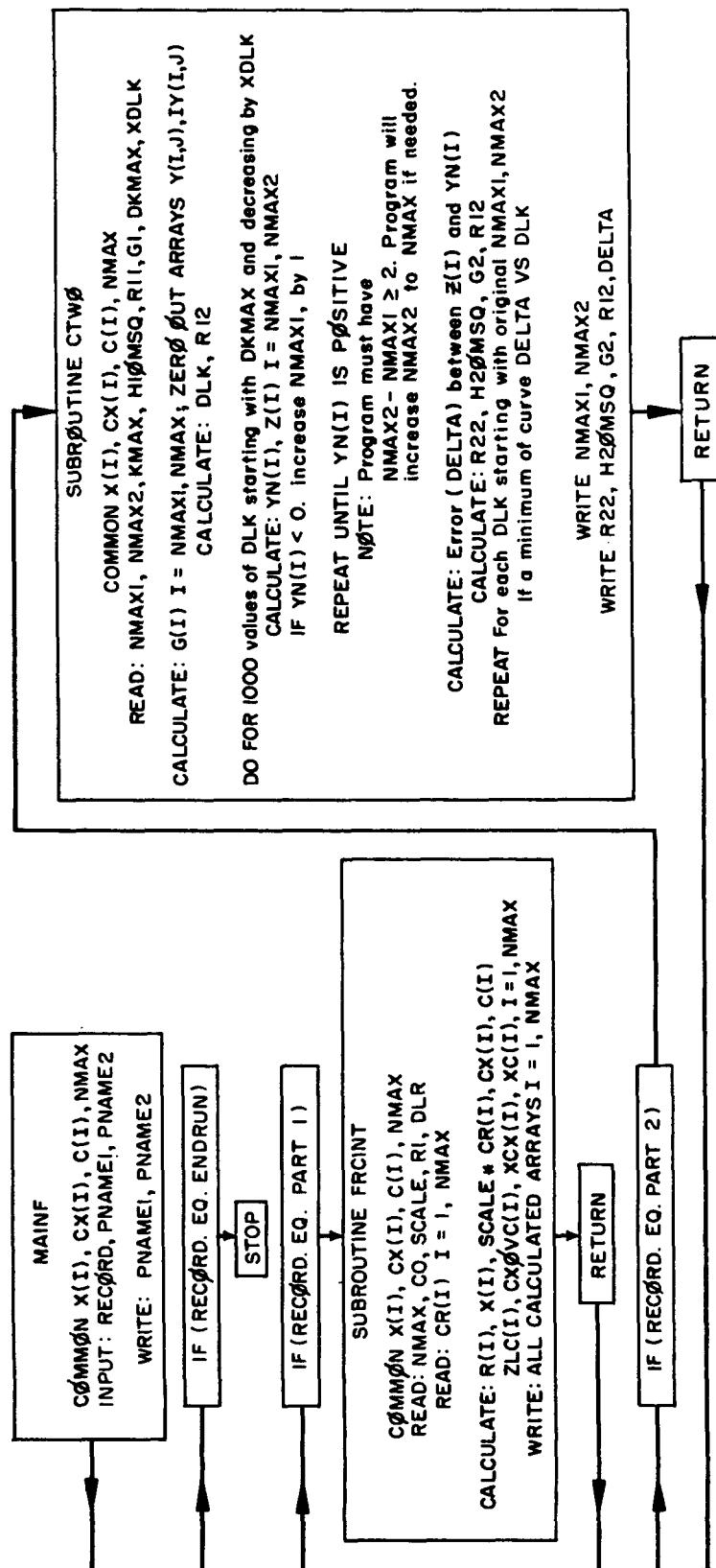


Figure 1. Computer Data Flow Diagram

COMPUTER PRINTOUT

```
$IBFTC MAINF DECK
  COMMON X,CX,C,NMAX
C  DIMENSIONS FOR COMMON
  DIMENSION X(100),CX(100),C(100)
  DATA P1,P2,P3/6HPART 1,6HENDRUN,6H
  DATA P4/6HPART 2/
1 READ(5,101) RECORD,PNAME1,PNAME2
101 FORMAT(A6,4X,2A6)
    IF(RECORD = P1) 2,10,2
    2 IF(RECORD = P2) 3,89,3
    3 IF(RECORD = P4) 4,11,4
    4 IF(RECORD = P3) 99,1,99
10 WRITE(6,1000)
1000 FORMAT(1H1/1HA)
    WRITE(6,2000) PNAME1,PNAME2
2000 FORMAT(1H ,50X,25HIDENTIFICATION NUMBER IS ,2A6)
    CALL FRCINT
    WRITE(6,1001)
1001 FORMAT(1HA/1HA)
    GO TO 1
11 WRITE(6,1000)
    WRITE(6,2000) PNAME1,PNAME2
    CALL CTWO
    WRITE(6,1001)
    GO TO 1
99 WRITE(6,3000) RECORD
3000 FORMAT(1H ,36HWHAT DO WE DO WITH THE CARD LABELED ,A6)
    GO TO 1
89 WRITE(6,1000)
    WRITE(6,7000)
7000 FORMAT(8(1H END OF RUN,3X)/1H1)
    STOP
    END
```

COMPUTER PRINTOUT (CONT)

```

$IBFTC FRCIN  DECK
      SUBROUTINE FRCINT
      COMMON X,CX,C,NMAX
C      DIMENSIONS FOR COMMON
      DIMENSION X(100),CX(100),C(100)
      DIMENSION CR(100),R(100),ZLC(100),CXOVC(100),XLX(100),XL(100)
      READ(5,101) NMAX,CO,SCALE,R1,DLR
101 FORMAT(13,1P2E11.4,0PF10.5,0PF10.6)
100 FORMAT(A6)
      READ(5,102) (CR(I),I = 1,NMAX)
102 FORMAT(16F5.0)
      DO 1 I = 1,NMAX
      R(I) = R1 + FLOAT(I-1)*DLR
      X(I) = R(I)**2
      CR(I) = SCALE*CR(I)
      CX(I) = CR(I)/(2.*R(I))
1 CONTINUE
      A = 0.
      COEF = 0.
      DO 2 I = 1,NMAX
      IF(I.EQ.1) GO TO 2
      DLX = X(I) - X(I-1)
      AVGCX = (CX(I)+CX(I-1))/2.
      COEF = COEF + DLX*AVGCX
      AC = (COEF + C(I-1))/2.
      A = A + DLX*AC
2 C(I) = COEF
      DIFBM = X(NMAX) - X(1)
      CM = (DIFBM*CO - A)/DIFBM
      WRITE(6,2000) CO,DIFBM,CM
2000 FORMAT(1H ,33HTHE CONCENTRATION FOR THIS RUN = ,E11.4/43H DIFFEREN
      1CF BTWN SQS OF BTM AND MENISCUS = ,E15.8/21H CONC. AT MENISCUS = ,
      2E11.4///)
      DO 3 I = 1,NMAX
      C(I) = C(I) + CM
      ZLC(I) = 0.
      IF(C(I).LE.0.) GO TO 3
      ZLC(I) = ALOG(C(I))
      CXOVC(I) = CX(I)/C(I)
      XCX(I) = 1./CX(I)
      XC(I) = 1./C(I)
3 CONTINUE
      WRITE(6,2001)
2001 FORMAT(1H ,1X,1HI,9X,1HR,11X,1HX,11X,2HCR,1CX,2HCX,10X,IHC,9X,5HLN
      1(C),7X,4HCX/C,8X,4H1/CX,8X,3H1/C//)
      DO 4 I = 1,NMAX
4 WRITE(6,2002) I,R(I),X(I),CR(I),CX(I),C(I),ZLC(I),CXOVC(I),XCX(I),
      1XC(I)
2002 FORMAT(1H ,I2,5X,9(1PE11.4,1X))
      RETURN
      END

```

COMPUTER PRINTOUT (CONT)

```

$IBFTC CTAU DECK
  SUBROUTINE CTWO
    COMMON X,CX,C,NMAX
    C   DIMENSIONS FOR COMMON
    DIMENSION X(100),CX(100),C(100)
    DIMENSION G(100),YN(100),U(100),Z(100)
    READ(5,100) NMAX1,NMAX2,KMAX,H1OMSQ,R11,G1,DKMAX,XDLK
100  FORMAT(3I3,3F10.3,F15.8,F10.6)
    DO 1 I = NMAX1,NMAX
    A1 = H1OMSQ*X(I) - R11*C(I)
    A2 = EXP(A1)
1  G(I) = G1*A2
    DO 2 K = 1,KMAX
    K1 = NMAX1
    K2 = NMAX2
    DLK = DKMAX + XDLK*FLOAT(K-1)
    WRITE(6,1001) DLK
1001 FORMAT(1H ,80X,5HKN = ,F10.5)
    R12 = R11 - DLK
    98 CONTINUE
    WRITE(6,2000) NMAX1,NMAX2
2000 FORMAT(1H ,8H NMAX1 = ,I2,9H NMAX2 = ,I2)
    DO 3 I = NMAX1,NMAX2
    A1 = C(I) - G(I)
    A2 = 1. + DLK*G(I)
    YN(I) = A1/A2
    IF(I.EQ.NMAX1) GO TO 20
    GO TO 21
20  A3 = X(I) - R12*C(I)/H1OMSQ
    XN1 = A3 - 1.
    21 CONTINUE
    U(I) = X(I) - (R12*C(I)/H1OMSQ) - XN1
    XXN = 1.
    IF(YN(I).LT.0.1E-05) GO TO 99
    IF(I.EQ.NMAX1) GO TO 22
    GO TO 23
22  A3 = ALOG(YN(I))
    XN2 = ABS(A3) - 1.
    23 CONTINUE
    Z(I) = ALOG(YN(I)) + XN2
    3 CONTINUE
    A1 = 0.
    A2 = 0.
    A3 = 0.
    A4 = 0.
    A5 = 0.
    A6 = 0.
    A7 = 0.
    A8 = 0.
    XN = FLOAT(NMAX2 - NMAX1 + 1)
    DO 4 I = NMAX1,NMAX2
    A1 = A1 + 0.1*U(I)
    A2 = A2 + (0.1*U(I))**2
    A3 = A3 + 100.*YN(I)

```

COMPUTER PRINTOUT (CONT)

```

A4 = A4 + (100.*YN(I))**2
A5 = A5 + Z(I)
A6 = A6 + 10.*U(I)*YN(I)
A7 = A7 + 0.1*U(I)*Z(I)
4 A8 = A8 + 100.*YN(I)*Z(I)
B1 = A2*A4 - A6*A6
B2 = A1*A4 - A3*A6
B3 = A2*A3 - A1*A6
DENOM = XN*B1 - A1*B2 - A3*B3
ANUM = A5*B1 - A7*B2 - A8*B3
B1 = A7*A4 - A8*A6
B2 = A5*A4 - A3*A8
B3 = A3*A7 - A5*A6
BNUM = XN*B1 - A1*B2 - A3*B3
B1 = A7*A6 - A2*A8
B2 = A5*A6 - A1*A8
B3 = A1*A7 - A5*A2
CNUM = XN*B1 - A1*B2 - A3*B3
H2OMSQ = 0.1*(BNUM/DENOM)
B = 100.* (CNUM/DENOM)
R22 = B + R12*H2OMSQ/H10MSQ
XK = CNUM/DENOM
XLNG2 = XK - XN1*H2OMSQ - XN2
WRITE(6,3001) DENOM,ANUM,BNUM,CNUM,R22,H2OMSQ,XLNG2
3001 FORMAT(1H ,7(1X,E15.8,1X))
IF(ABS(XLNG2).GT.88.) GO TO 40
G2 = EXP(XLNG2)
GO TO 41
40 G2 = 0.
41 CONTINUE
COEF = 0.
DO 5 I = NMAX1,NMAX2
B1 = XK
B2 = H2OMSQ*U(I)
B3 = B*YN(I)
5 COEF = COEF + (Z(I)-B1-B2+B3)**2
DELTA = COEF/XN
IF(H2OMSQ.LT.0.) GO TO 32
WRITE(6,1000) K,R12,G2,H2OMSQ,R22,DELTA
1000 FORMAT(1H ,5X,I2,7H R12 = ,1PE10.3,6H G2 = ,1PE10.3,10H H2OMSQ = ,
11PE10.3,7H R22 = ,1PE10.3,9H DELTA = ,1PE10.3/)
32 CONTINUE
NMAX1 = K1
NMAX2 = K2
GO TO 2
99 CONTINUE
NMAX1 = NMAX1 + 1
IF((NMAX2-NMAX1).GT.2) GO TO 97
NMAX2 = NMAX2 + 1
IF(NMAX2.EQ.NMAX) GO TO 88
97 GO TO 98
2 CONTINUE
88 RETURN
END

```

SECTION VII

REFERENCES

1. H. Fujita, "Mathematical Theory of Sedimentation Analysis," Academic Press, New York, 1962.
2. E. F. Casassa, "Sedimentation Equilibrium in Multicomponent Solutions," (Private Communication).
3. M. Gehatia and D. R. Wiff, AFML-TR-67-121, Part II.
4. M. Gehatia, AFML-TR-67-121, Part I.

TABLE I

EXPERIMENTAL DATA FOR SAMPLE 1 AT ROTOR SPEED 10,589 RPM
(See Figure 2a)

THE CONCENTRATION FOR THIS RUN = 1.1394×10^{-6}
THE DIFFERENCE BTWN SOS OF BTW AND MENSCUS = $0.93875737 \times 10^{-6}$
CONE. AT MENISCUS = 1.10846×10^{-6}

Identification Number is Sample 1 10,589 RPM

T	R	X	C _R	C _X	C	C _{N(C)}	C _{X/C}	1/CX	C _{X/C}	1/CX	1/C
1	6.5295E-00	4.2634E-01	3.9547E-02	2.9519E-03	1.0837E-01	-2.2222E-00	2.7237E-02	3.3878E-02	9.2272E-00	9.2272E-00	9.2272E-00
2	6.5413E-01	4.2794E-01	3.9548E-02	3.0950E-03	1.0835E-01	-2.2179E-00	2.7785E-02	3.3069E-02	9.1882E-00	9.1882E-00	9.1882E-00
3	6.5531E-01	4.2964E-01	4.0575E-02	3.0950E-03	1.0931E-01	-2.2136E-00	2.8324E-02	3.2300E-02	9.1486E-00	9.1486E-00	9.1486E-00
4	6.5649E-01	4.3170E-01	4.1692E-02	3.1754E-03	1.0979E-01	-2.2092E-00	2.8922E-02	3.1492E-02	9.1082E-00	9.1082E-00	9.1082E-00
5	6.5766E-01	4.3252E-01	4.2809E-02	3.2545E-03	1.1229E-01	-2.2047E-00	2.9509E-02	3.0766E-02	9.0671E-00	9.0671E-00	9.0671E-00
6	6.5884E-01	4.3447E-01	4.3924E-02	3.3334E-03	1.1080E-01	-2.2000E-00	3.0085E-02	2.9999E-02	9.0253E-00	9.0253E-00	9.0253E-00
7	6.6002E-01	4.3552E-01	4.5454E-02	3.4427E-03	1.1133E-01	-2.1953E-00	3.0925E-02	2.9047E-02	8.9826E-00	8.9826E-00	8.9826E-00
8	6.6119E-01	4.3719E-01	4.6865E-02	3.5440E-03	1.1187E-01	-2.1904E-00	3.1680E-02	2.8217E-02	8.9390E-00	8.9390E-00	8.9390E-00
9	6.6237E-01	4.3874E-01	4.8154E-02	3.6815E-03	1.2434E-01	-2.1854E-00	3.2691E-02	2.7207E-02	8.8942E-00	8.8942E-00	8.8942E-00
10	6.6355E-01	4.4033E-01	5.0213E-02	3.7836E-03	1.3101E-01	-2.1802E-00	3.3479E-02	2.6430E-02	8.8484E-00	8.8484E-00	8.8484E-00
11	6.6473E-01	4.4186E-01	5.1937E-02	3.9677E-03	1.3632E-01	-2.1749E-00	3.4385E-02	2.5597E-02	8.8016E-00	8.8016E-00	8.8016E-00
12	6.6591E-01	4.4343E-01	5.3695E-02	4.0445E-03	1.4695E-01	-2.1695E-00	3.5403E-02	2.4725E-02	8.7536E-00	8.7536E-00	8.7536E-00
13	6.6709E-01	4.4501E-01	5.5935E-02	4.1994E-03	1.4894E-01	-2.1638E-00	3.6466E-02	2.3879E-02	8.7043E-00	8.7043E-00	8.7043E-00
14	6.6926E-01	4.4655E-01	5.8124E-02	4.3414E-03	1.1556E-01	-2.1580E-00	3.7569E-02	2.3034E-02	8.6538E-00	8.6538E-00	8.6538E-00
15	6.6944E-01	4.4815E-01	6.357E-02	4.5080E-03	1.1625E-01	-2.1520E-00	3.8777E-02	2.2183E-02	8.6019E-00	8.6019E-00	8.6019E-00
16	6.7162E-01	4.4973E-01	6.6597E-02	4.6740E-03	1.1698E-01	-2.1458E-00	3.9157E-02	2.1395E-02	8.5486E-00	8.5486E-00	8.5486E-00
17	6.7179E-01	4.5131E-01	6.9523E-02	4.8395E-03	1.1773E-01	-2.1394E-00	4.1107E-02	2.0663E-02	8.4940E-00	8.4940E-00	8.4940E-00
18	6.7297E-01	4.5289E-01	6.7557E-02	5.0277E-03	1.1851E-01	-2.1327E-00	4.2418E-02	1.9489E-02	8.4380E-00	8.4380E-00	8.4380E-00
19	6.7415E-01	4.5454E-01	7.3199E-02	5.2213E-03	1.1932E-01	-2.1259E-00	4.3757E-02	1.9152E-02	8.3805E-00	8.3805E-00	8.3805E-00
20	6.7531E-01	4.5627E-01	7.6137E-02	5.4213E-03	1.2017E-01	-2.1189E-00	4.4993E-02	1.8493E-02	8.3216E-00	8.3216E-00	8.3216E-00
21	6.7551E-01	4.5795E-01	7.6292E-02	5.6230E-03	1.2105E-01	-2.1116E-00	4.6453E-02	1.7784E-02	8.2612E-00	8.2612E-00	8.2612E-00
22	6.7769E-01	4.5952E-01	7.9322E-02	5.8303E-03	1.2196E-01	-2.1041E-00	4.7805E-02	1.7152E-02	8.1993E-00	8.1993E-00	8.1993E-00
23	6.7936E-01	4.6158E-01	8.2165E-02	6.0518E-03	1.2291E-01	-2.0963E-00	4.9237E-02	1.6552E-02	8.1360E-00	8.1360E-00	8.1360E-00
24	6.8144E-01	4.6245E-01	8.5209E-02	6.2502E-03	1.2390E-01	-2.0883E-00	5.0567E-02	1.5962E-02	8.0713E-00	8.0713E-00	8.0713E-00
25	6.8122E-01	4.6417E-01	8.8616E-02	6.5223E-03	1.2492E-01	-2.0801E-00	5.2211E-02	1.5332E-02	8.0051E-00	8.0051E-00	8.0051E-00
26	6.8230E-01	4.6566E-01	9.2112E-02	6.7537E-03	1.2599E-01	-2.0716E-00	5.3685E-02	1.4785E-02	7.9373E-00	7.9373E-00	7.9373E-00
27	6.8357E-01	4.6727E-01	9.6267E-02	7.0144E-03	1.2626E-01	-2.0716E-00	5.5201E-02	1.4202E-02	7.8679E-00	7.8679E-00	7.8679E-00
28	6.8475E-01	4.6884E-01	1.0122E-01	7.3182E-03	1.2826E-01	-2.0537E-00	5.7060E-02	1.3666E-02	7.7969E-00	7.7969E-00	7.7969E-00
29	6.8593E-01	4.7052E-01	1.0294E-01	7.5866E-03	1.2946E-01	-2.0444E-00	5.8603E-02	1.3181E-02	7.745E-00	7.745E-00	7.745E-00
31	6.8711E-01	4.7211E-01	1.0451E-01	7.8936E-03	1.3071E-01	-2.0348E-00	6.0314E-02	1.2685E-02	7.6506E-00	7.6506E-00	7.6506E-00
32	6.8929E-01	4.8193E-01	1.0651E-01	8.2123E-03	1.2492E-01	-2.0249E-00	6.1221E-02	1.2225E-02	7.5752E-00	7.5752E-00	7.5752E-00
33	6.9146E-01	4.8336E-01	1.0856E-01	8.4746E-03	1.3136E-01	-2.0147E-00	6.3546E-02	1.1800E-02	7.4984E-00	7.4984E-00	7.4984E-00
34	6.9371E-01	4.8698E-01	1.1042E-01	8.7937E-03	1.3476E-01	-2.0042E-00	6.5230E-02	1.1376E-02	7.4203E-00	7.4203E-00	7.4203E-00
35	6.9593E-01	4.7752E-01	1.1259E-01	9.1259E-03	1.3652E-01	-1.9935E-00	6.8444E-02	1.0982E-02	7.3410E-00	7.3410E-00	7.3410E-00
36	6.9817E-01	4.8074E-01	1.1416E-01	9.3466E-03	1.3773E-01	-1.9924E-00	7.0438E-02	1.0592E-02	7.2603E-00	7.2603E-00	7.2603E-00
37	6.9935E-01	4.8315E-01	1.1575E-01	9.8054E-03	1.3913E-01	-1.9711E-00	7.0387E-02	1.0198E-02	7.1784E-00	7.1784E-00	7.1784E-00
38	6.9971E-01	4.8679E-01	1.1695E-01	1.0121E-01	1.3947E-01	-1.9594E-00	7.2453E-02	9.7926E-02	7.0950E-00	7.0950E-00	7.0950E-00
39	6.9971E-01	4.88679E-01	1.1819E-01	1.0321E-01	1.4177E-01	-1.9473E-00	7.4425E-02	9.4189E-02	7.0101E-00	7.0101E-00	7.0101E-00
40	6.9971E-01	4.9064E-01	1.1939E-01	1.0521E-01	1.4443E-01	-1.9350E-00	7.6355E-02	9.6679E-02	7.9238E-00	7.9238E-00	7.9238E-00
41	7.0076E-01	4.9274E-01	1.2059E-01	1.0721E-01	1.4628E-01	-1.9223E-00	7.9043E-02	1.0592E-02	8.3664E-00	8.3664E-00	8.3664E-00
42	7.0171E-01	4.9484E-01	1.2179E-01	1.0921E-01	1.4825E-01	-1.9092E-00	8.0664E-02	1.0387E-02	8.1961E-00	8.1961E-00	8.1961E-00
43	7.0276E-01	4.9694E-01	1.2295E-01	1.1121E-01	1.5022E-01	-1.8857E-00	8.3011E-02	1.0183E-02	8.6571E-00	8.6571E-00	8.6571E-00
44	7.0381E-01	4.9904E-01	1.2405E-01	1.1321E-01	1.5222E-01	-1.8618E-00	8.5329E-02	9.6938E-02	8.6651E-00	8.6651E-00	8.6651E-00
45	7.0487E-01	5.0114E-01	1.2515E-01	1.1521E-01	1.5432E-01	-1.8374E-00	8.7799E-02	9.4189E-02	7.3710E-00	7.3710E-00	7.3710E-00
46	7.0595E-01	5.0324E-01	1.2625E-01	1.1721E-01	1.5632E-01	-1.8137E-00	9.0250E-02	9.0535E-02	6.3167E-00	6.3167E-00	6.3167E-00
47	7.0713E-01	5.0533E-01	1.2735E-01	1.1921E-01	1.5832E-01	-1.7894E-00	9.2950E-02	9.1734E-02	6.2803E-00	6.2803E-00	6.2803E-00
48	7.0831E-01	5.0743E-01	1.2845E-01	1.2121E-01	1.6032E-01	-1.7651E-00	9.5783E-02	9.0217E-02	6.1824E-00	6.1824E-00	6.1824E-00
49	7.0949E-01	5.0953E-01	1.2955E-01	1.2321E-01	1.6232E-01	-1.7417E-00	9.8660E-02	9.4839E-02	6.0830E-00	6.0830E-00	6.0830E-00
50	7.1067E-01	5.1163E-01	1.3065E-01	1.2521E-01	1.6439E-01	-1.7187E-00	1.0178E-01	9.1788E-01	5.9820E-01	5.9820E-01	5.9820E-01

TABLE I (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1266E-00	5.0534E-01	2.5363E-01	1.7843E-C2	1.7008E-01	-1.7715E-00	1.0490E-01	5.6046E-01	5.8795E-00
51	7.1184E-00	5.2672E-01	2.6374E-01	1.8526E-C2	1.7313E-01	-1.7537E-00	1.0700E-01	5.3980E-01	5.7760E-00
52	7.11302E-00	5.0839E-01	2.7997E-01	1.9633E-C2	1.7633E-01	-1.7354E-00	1.1134E-01	5.0934E-01	5.6711E-00
53	7.1420E-00	5.1018E-01	2.9615E-01	2.06666E-02	1.7972E-01	-1.7164E-00	1.1499E-01	4.8389E-01	5.5642E-00
54	7.1537E-00	5.1176E-01	3.1955E-01	2.2334E-02	1.8334E-01	-1.664E-00	1.2182E-01	4.4776E-01	5.4544E-00
55	7.1655E-00	5.1345E-01	3.4997E-01	2.4420E-02	1.8728E-01	-1.6751E-00	1.3039E-01	4.0950E-01	5.3396E-00
56	7.1773E-00	5.1513E-01	3.8547E-01	2.6854E-02	1.9161E-01	-1.623E-00	1.4015E-01	3.7239E-01	5.2189E-00
57	7.1891E-00	5.1683E-01	4.5644E-01	3.1748E-02	1.9657E-01	-1.6267E-00	1.6151E-01	3.1498E-01	5.0372E-00
58	7.2020E-00	5.1852E-01	5.4270E-01	3.7683E-02	2.0245E-01	-1.572E-00	1.8613E-01	2.6537E-01	4.9394E-00
59	7.2126E-00	5.2022E-01	8.3691E-01	5.8156E-02	2.1059E-01	-1.5578E-00	2.7616E-01	1.7195E-01	4.7486E-00

TABLE II
EXPERIMENTAL DATA FOR SAMPLE 1 AT ROTOR SPEED 8,766 RPM
(See Figure 2b)

THE CONCENTRATION FOR THIS RUN = 3.1394×10^{-6}
DIFFERENCE ATWN SOS OF RT4 AND MENISCUS = $0.939875737 \times 10^{-6}$
CONC. AT MENISCUS = 2.1152×10^{-6}

Identification Number is Sample 1 8,766 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.5413F 70	4.2634F 01	3.2461E-02	2.4857E-03	1.1523E-01	-2.1608E 00	2.1572E-02	4.0230E 02	8.6783E 00
2	6.5413F 70	3.3475E-02	2.5598E-03	1.1562E-01	-2.1575E 00	2.2131E-02	3.9081E 02	8.6492E 00	
3	6.5531F 50	4.2933F 01	3.4492E-02	2.6316E-03	1.1602E-01	-2.1540E 00	2.2682E-02	3.8000E 02	8.6193E 00
4	6.5548E 50	4.3277E 01	3.5524E-02	2.7041E-03	1.1643E-01	-2.1505E 00	2.3225E-02	3.6981E 02	8.5888E 00
5	6.5766E 50	4.3277E 01	3.6519E-02	2.8468E-03	1.1685E-01	-2.1468E 00	2.3759E-02	3.6018E 02	8.5576E 00
6	6.5944E 50	4.3477E 01	3.7533E-02	2.9202E-03	1.1729E-01	-2.1431E 00	2.4285E-02	3.5107E 02	8.5258E 00
7	6.6122E 50	4.3562E 01	3.8547E-02	2.9920E-03	1.1774E-01	-2.1393E 00	2.4802E-02	3.4245E 02	8.4934E 00
8	6.6119E 50	4.3718E 01	3.9866E-02	3.0147E-03	1.1820E-01	-2.1354E 00	2.5505E-02	3.3171E 02	8.6022E 00
9	6.5237E 50	4.3874E 01	4.1083E-02	3.0412E-03	1.1868E-01	-2.1313E 00	2.6132E-02	3.2245E 02	8.4262E 00
10	6.61355E 50	4.4033E 01	4.2625E-02	3.2104E-03	1.1917E-01	-2.1272E 00	2.6939E-02	3.1149E 02	8.3914E 00
11	6.6473E 50	4.4186E 01	4.3924E-02	3.3039E-03	1.1968E-01	-2.1229E 00	2.7606E-02	3.0288E 02	8.3556E 00
12	6.6591E 50	4.4434E 01	4.5649E-02	3.4275E-03	1.2021E-01	-2.1185E 00	2.9173E-02	2.9173E 02	8.390E 00
13	6.5778E 50	4.4575E 01	4.7372E-02	3.5557E-03	1.2075E-01	-2.1140E 00	2.9404E-02	2.8163E 02	8.2812E 00
14	6.5326E 50	4.4657E 01	4.8793E-02	3.6507E-03	1.2132E-01	-2.1093E 00	3.0091E-02	2.7392E 02	8.2426E 00
15	6.6944E 50	4.4815E 01	5.0729E-02	3.7882E-03	1.2191E-01	-2.1045E 00	3.1075E-02	2.6397E 02	8.2030E 00
16	6.7052E 50	4.4973E 01	5.2343E-02	3.9726E-03	1.2251E-01	-2.0995E 00	3.2251E-02	2.5624E 02	8.1623E 00
17	6.7179E 50	4.5111E 01	5.4372E-02	4.0468E-03	1.2314E-01	-2.0944E 00	3.2862E-02	2.4711E 02	8.1207E 00
18	6.7207E 50	4.5294E 01	5.6502E-02	4.1979E-03	1.2380E-01	-2.0891E 00	3.3910E-02	2.3821E 02	8.0778E 00
19	6.7415F 50	4.5448E 01	5.8632E-02	4.3486E-03	1.2447E-01	-2.0837E 00	3.4936E-02	2.2995E 02	8.0338E 00
20	6.7533F 50	4.5675E 01	6.6661E-02	4.4912E-03	1.2518E-01	-2.0780E 00	3.5879E-02	2.2266E 02	7.9888E 00
21	6.7551F 50	4.5766E 01	6.2791E-02	4.6494E-03	1.2590E-01	-2.0722E 00	3.6861E-02	2.1548E 02	7.9426E 00
22	6.7768F 50	4.5925E 01	6.4922E-02	4.7900E-03	1.2666E-01	-2.0663E 00	3.7819E-02	2.0877E 02	7.8955E 00
23	6.7896F 50	4.6085E 01	6.6950E-02	4.9311E-03	1.2743E-01	-2.0602E 00	3.8696E-02	2.0289E 02	7.8473E 00
24	6.8744E 50	4.6544E 01	5.9182E-02	5.3666E-03	1.2823E-01	-2.0539E 00	3.9667E-02	1.9659E 02	7.7983E 00
25	6.8122F 50	4.6644E 01	7.1920E-02	5.2714E-03	1.2906E-01	-2.0474E 00	4.0843E-02	1.8970E 02	7.7481E 00
26	6.8219E 50	4.6566E 01	7.4511E-02	5.4258E-03	1.2992E-01	-2.0408E 00	4.1762E-02	1.8430E 02	7.6969E 00
27	6.8357E 50	4.6727E 01	7.6597E-02	5.6022E-03	1.3040E-01	-2.0340E 00	4.2856E-02	1.7851E 02	7.6447E 00
28	6.8475E 50	4.6884E 01	7.9123E-02	5.7775E-03	1.3173E-01	-2.0279E 00	4.3860E-02	1.7368E 02	7.5915E 00
29	6.8593E 50	4.7050E 01	8.1964E-02	5.9746E-03	1.3268E-01	-2.0198E 00	4.5032E-02	1.6737E 02	7.5312E 00
30	6.8744E 50	4.7211F 01	8.4702E-02	6.1637E-03	1.3366E-01	-2.0125E 00	4.6116E-02	1.6224E 02	7.4818E 00
31	5.8378E 50	4.7373E 01	8.7543E-02	6.3595E-03	1.3467E-01	-2.0047E 00	4.7047E-02	1.5722E-02	7.4255E 00
32	5.9946E 50	4.7536E 01	9.3933E-02	6.5554E-03	1.3572E-01	-1.9972E 00	4.8229E-02	1.5259E-02	7.3682E 00
33	5.9554E 50	4.7639E 01	9.3932E-02	6.7931E-03	1.3680E-01	-1.9992E 00	4.9656E-02	1.4721E 02	7.3097E 00
34	6.0192E 50	4.7861E 01	9.6977E-02	7.0388E-03	1.3793E-01	-1.981CE 00	5.0815E-02	1.4268E 02	7.2502E 00
35	6.9378E 50	4.8244E 01	1.0243E-01	8.5273E-03	1.4554E-01	-1.9273E 00	5.2094E-02	1.3801E 02	7.1899E 00
36	5.9447E 50	4.8198E 01	1.0387E-01	7.4819E-03	1.4697E-01	-1.9175E 00	5.3333E-02	1.3361E 02	7.1279E 00
37	6.9515E 50	4.9311E 01	1.0753F-01	7.7319E-03	1.4154E-01	-1.9552E 00	5.4627E-02	1.2934E 02	7.0652E 00
38	6.9553E 50	4.8515E 01	1.1139E-01	7.9954E-03	1.4283E-01	-1.9461E 00	5.5980E-02	1.2509E 02	7.0015E 00
39	6.9771F 50	4.8673E 01	1.1534E-01	1.0619E-01	1.4416E-01	-1.9368E 00	5.7334E-02	1.2099E 02	6.9366E 00
40	6.7388E 50	4.8844E 01	1.1919E-01	8.5273E-03	1.4554E-01	-1.9273E 00	5.8589E-02	1.1727E 02	6.8708E 00
41	7.0176F 50	4.9049F 01	1.2345E-01	8.9175E-03	1.4697E-01	-1.9175E 00	5.9993E-02	1.1361E 02	6.8040E 00
42	7.0124F 50	4.9174E 01	1.2771E-01	9.1062E-03	1.4745E-01	-1.9075E 00	6.1341E-02	1.0981E 02	6.7362E 00
43	7.0242F 50	4.9332E 01	1.3197F-01	9.3942E-03	1.4998E-01	-1.8972E 00	6.2636E-02	1.0645E 02	6.6675E 00
44	7.0316E 50	4.9515E 01	1.3694E-01	9.7311E-03	1.5156E-01	-1.8867E 00	6.4209E-02	1.0276E 02	6.5979E 00
45	6.9378E 50	4.9671E 01	1.4202F-01	1.0707F-02	1.5321E-01	-1.8760E 00	6.5763E-02	9.5933E 01	6.2271E 00
46	7.0505E 50	4.9817E 01	1.4739E-01	1.1741E-02	1.5456E-01	-1.8649E 00	6.7250E-02	9.5544E 01	6.0554E 00
47	7.0712F 50	5.0023E 01	1.5226E-01	1.2766E-02	1.5667E-01	-1.8536E 00	6.8711E-02	9.3884E 01	6.3827E 00
48	7.0931F 50	5.1767E 01	1.5825E-01	1.1171E-02	1.5850E-01	-1.8420E 00	7.0478E-02	8.9519E 01	6.2091E 00
49	7.0349F 50	5.2337E 01	1.6447E-01	1.0540E-01	1.6040E-01	-1.8301E 00	7.2201E-02	8.6347E 01	6.2334E 00

TABLE II (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1266E-20	5.2574E-01	1.7793E-01	1.2026E-02	1.6237E-01	-1.8178E-00	7.4062E-02	8.3154E-01	6.1586E-00
51	7.1194E-00	5.1672E-01	1.7853E-01	1.2547E-02	1.6443E-01	-1.8051E-00	7.6264E-02	7.9743E-01	6.0815E-00
52	7.1352E-00	5.0839E-01	1.8746E-01	1.3146E-02	1.6659E-01	-1.7922E-00	7.8911E-02	7.6071E-01	6.0028E-00
53	7.1427E-00	5.1008E-01	1.9791E-01	1.3855E-02	1.6886E-01	-1.7787E-00	8.2054E-02	7.2174E-01	5.9222E-00
54	7.1537E-00	5.1117E-01	2.1211E-01	1.4825E-02	1.7127E-01	-1.7645E-00	8.6559E-02	6.7453E-01	5.8387E-00
55	7.1555E-00	5.1345E-01	2.2824E-01	1.5926E-02	1.7387E-01	-1.7493E-00	9.1601E-02	6.2789E-01	5.7516E-00
56	7.1773E-00	5.1513E-01	2.4854E-01	1.7313E-02	1.7667E-01	-1.7335E-00	9.7997E-02	5.7758E-01	5.6602E-00
57	7.1991E-00	5.1683E-01	2.8719E-01	1.9966E-02	1.7983E-01	-1.7158E-00	1.1103E-01	5.0085E-01	5.5609E-00
58	7.2078E-00	5.1852E-01	3.7229E-01	2.5850E-02	1.9371E-01	-1.6944E-00	1.4071E-01	3.8685E-01	5.4434E-00
59	7.2126E-00	5.2022E-01	5.3255E-01	3.6919E-02	1.8904E-01	-1.6658E-00	1.9530E-01	2.7087E-01	5.2900E-00

TABLE III
EXPERIMENTAL DATA FOR SAMPLE 1 AT ROTOR SPEED 7,447 RPM
(See Figure 2e)

I	R	X	CR	CX	C	LN(C)	1/CX	CX/C	1/CX	3.5431E-02	8.3336E-00
1	6.5205E-00	4.2634E-01	3.6518E-02	2.7964E-03	1.2000E-01	-2.1203E-00	2.3304E-02	3.4229E-02	8.2129E-02	3.5431E-02	8.3037E-00
2	6.5413E-00	3.2788E-01	3.6924E-02	2.8224E-03	1.2043E-01	-2.1167E-00	2.3436E-02	3.4541E-02	8.2037E-02	3.5431E-02	8.2037E-00
3	6.5531E-00	4.2943E-01	3.7431E-02	2.8560E-03	1.2087E-01	-2.1131E-00	2.3630E-02	3.5014E-02	8.2136E-02	3.5014E-02	8.2136E-00
4	6.5644E-00	4.3097E-01	3.7937E-02	2.8818E-03	1.2131E-01	-2.1094E-00	2.3756E-02	3.4700E-02	8.2444E-02	3.4700E-02	8.2444E-00
5	6.5766E-00	4.3252E-01	3.8547E-02	2.9306E-03	1.2176E-01	-2.1057E-00	2.4069E-02	3.4122E-02	8.2129E-02	3.4122E-02	8.2129E-00
6	6.5884E-00	4.3407E-01	3.9554E-02	2.9639E-03	1.2222E-01	-2.1020E-00	2.4251E-02	3.3740E-02	8.1822E-02	3.4251E-02	8.1822E-00
7	6.6007E-00	4.3552E-01	3.9562E-02	2.9970E-03	1.2268E-01	-2.0982E-00	2.4430E-02	3.3367E-02	8.1513E-02	3.4430E-02	8.1513E-00
8	6.6119E-00	4.3718E-01	4.0373E-02	3.0530E-03	1.2315E-01	-2.0943E-00	2.4791E-02	3.2754E-02	8.1202E-02	3.4791E-02	8.1202E-00
9	6.6231E-00	4.3874E-01	4.0383E-02	3.1012E-03	1.2341E-01	-2.0905E-00	2.5075E-02	3.2245E-02	8.0886E-02	3.2245E-02	8.0886E-00
10	6.6355E-00	4.4032E-01	4.1692E-02	3.1416E-03	1.2412E-01	-2.0865E-00	2.5311E-02	3.1831E-02	8.0569E-02	3.1831E-02	8.0569E-00
11	6.6443E-00	4.4186E-01	4.2675E-02	3.2047E-03	1.2461E-01	-2.0825E-00	2.5717E-02	3.1204E-02	8.0248E-02	3.1204E-02	8.0248E-00
12	6.6559E-00	4.4343E-01	4.3518E-02	3.2676E-03	1.2512E-01	-2.0785E-00	2.6115E-02	3.0644E-02	7.9933E-02	3.0644E-02	7.9933E-00
13	6.6701E-00	4.4505E-01	4.4431E-02	3.3302E-03	1.2564E-01	-2.0743E-00	2.6506E-02	3.0298E-02	7.9593E-02	3.0298E-02	7.9593E-00
14	6.6826E-00	4.4657E-01	4.5141E-02	3.3775E-03	1.2617E-01	-2.0702E-00	2.6770E-02	2.9608E-02	7.9260E-02	2.6770E-02	7.9260E-00
15	6.6944E-00	4.4815E-01	4.5952E-02	3.4322E-03	1.2670E-01	-2.0659E-00	2.7088E-02	2.9136E-02	7.8925E-02	2.7088E-02	7.8925E-00
16	6.7052E-00	4.4973E-01	4.6764E-02	3.4866E-03	1.2725E-01	-2.0616E-00	2.7400E-02	2.8681E-02	7.8586E-02	2.7400E-02	7.8586E-00
17	6.7170E-00	4.5131E-01	4.7778E-02	3.5580E-03	1.2781E-01	-2.0572E-00	2.7824E-02	2.8211E-02	7.8244E-02	2.7824E-02	7.8244E-00
18	6.7227E-00	4.5289E-01	4.8691E-02	3.6176E-03	1.2837E-01	-2.0528E-00	2.8180E-02	2.7642E-02	7.7897E-02	2.8180E-02	7.7897E-00
19	6.7415E-00	4.5544E-01	4.9706E-02	3.6865E-03	1.2895E-01	-2.0483E-00	2.8588E-02	2.7126E-02	7.7547E-02	2.8588E-02	7.7547E-00
20	6.7533E-00	4.5672E-01	4.9720E-02	3.7552E-03	1.2952E-01	-2.0437E-00	2.8988E-02	2.6632E-02	7.7193E-02	2.8988E-02	7.7193E-00
21	6.7651E-00	4.5766E-01	5.1734E-02	3.8236E-03	1.3015E-01	-2.0391E-00	2.9379E-02	2.6153E-02	7.6633E-02	2.9379E-02	7.6633E-00
22	6.7764E-00	4.5926E-01	5.2749E-02	3.8919E-03	1.3076E-01	-2.0344E-00	2.9763E-02	2.5695E-02	7.6474E-02	2.9763E-02	7.6474E-00
23	6.7885E-00	4.6085E-01	5.3763E-02	3.9598E-03	1.3139E-01	-2.0296E-00	3.0138E-02	2.5134E-02	7.6109E-02	3.0138E-02	7.6109E-00
24	6.8004E-00	4.6245E-01	5.4879E-02	4.0350E-03	1.3203E-01	-2.0247E-00	3.0561E-02	2.4783E-02	7.5740E-02	3.0561E-02	7.5740E-00
25	6.8122E-00	4.6406E-01	5.5995E-02	4.1099E-03	1.3268E-01	-2.0197E-00	3.0975E-02	2.4331E-02	7.5367E-02	3.0975E-02	7.5367E-00
26	6.8239E-00	4.6565E-01	5.7111E-02	4.1846E-03	1.3335E-01	-2.0148E-00	3.1381E-02	2.3897E-02	7.4991E-02	3.1381E-02	7.4991E-00
27	6.8357E-00	4.6727E-01	5.8249E-02	4.2788E-03	1.3403E-01	-2.0097E-00	3.1788E-02	2.3398E-02	7.4410E-02	3.1788E-02	7.4410E-00
28	6.8475E-00	4.6888E-01	5.9748E-02	4.3628E-03	1.3473E-01	-2.0045E-00	3.2383E-02	2.2921E-02	7.4225E-02	3.2383E-02	7.4225E-00
29	6.8593E-00	4.7052E-01	6.0864E-02	4.4366E-03	1.3544E-01	-2.0004E-00	3.2758E-02	2.2540E-02	7.3836E-02	3.2758E-02	7.3836E-00
30	6.8711E-00	4.7211E-01	6.2396E-02	4.5397E-03	1.3616E-01	-1.9939E-00	3.3141E-02	2.2028E-02	7.3442E-02	3.3141E-02	7.3442E-00
31	6.8828E-00	4.7373E-01	6.3877E-02	4.6425E-03	1.3691E-01	-1.9885E-00	3.3910E-02	2.1540E-02	7.3043E-02	3.3910E-02	7.3043E-00
32	6.8946E-00	4.7536E-01	6.5124E-02	4.7228E-03	1.3767E-01	-1.9829E-00	3.4307E-02	2.1174E-02	7.2640E-02	3.4307E-02	7.2640E-00
33	6.9064E-00	4.7698E-01	6.6495E-02	4.8429E-03	1.3847E-01	-1.9773E-00	3.5011E-02	2.0631E-02	7.2232E-02	3.5011E-02	7.2232E-00
34	6.9182E-00	4.7861E-01	6.8575E-02	4.9634E-03	1.3924E-01	-1.9715E-00	3.5646E-02	2.0148E-02	7.1817E-02	3.5646E-02	7.1817E-00
35	6.9301E-00	4.8024E-01	7.0624E-02	5.0940E-03	1.3990E-01	-1.9657E-00	3.6370E-02	1.9631E-02	7.1397E-02	3.6370E-02	7.1397E-00
36	6.9417E-00	4.8189E-01	7.2532E-02	5.2242E-03	1.3990E-01	-1.9597E-00	3.7076E-02	1.9142E-02	7.0970E-02	3.7076E-02	7.0970E-00
37	6.9535E-00	4.9351E-01	7.4653E-02	5.3685E-03	1.4177E-01	-1.9535E-00	3.7867E-02	1.8627E-02	7.0536E-02	3.7867E-02	7.0536E-00
38	6.9653E-00	4.9515E-01	7.6768E-02	5.5775E-03	1.4367E-01	-1.9473E-00	3.8574E-02	1.8094E-02	7.0094E-02	3.8574E-02	7.0094E-00
39	6.9771E-00	4.9679E-01	7.9225E-02	5.6775E-03	1.4535E-01	-1.9408E-00	3.9541E-02	1.7613E-02	6.9645E-02	3.9541E-02	6.9645E-00
40	6.9888E-00	4.9844E-01	8.1952E-02	5.8566E-03	1.4653E-01	-1.9342E-00	4.0521E-02	1.7075E-02	6.9198E-02	4.0521E-02	6.9198E-00
41	7.0007E-00	4.9929E-01	9.4550E-02	6.0351E-03	1.4751E-01	-1.9275E-00	4.1475E-02	1.6570E-02	6.8722E-02	4.1475E-02	6.8722E-00
42	7.0124E-00	4.0174E-01	10.7239E-02	6.2203E-03	1.4863E-01	-1.9206E-00	4.2452E-02	1.6076E-02	6.8247E-02	4.2452E-02	6.8247E-00
43	7.0242E-00	4.9339E-01	8.9774E-02	6.39n6E-03	1.4757E-01	-1.9135E-00	4.3305E-02	1.5649E-02	6.7765E-02	4.3305E-02	6.7765E-00
44	7.0362E-00	4.9505E-01	9.2513E-02	6.5775E-03	1.4846E-01	-1.9062E-00	4.4229E-02	1.5211E-02	6.7276E-02	4.4229E-02	6.7276E-00
45	7.0477E-00	4.9671E-01	9.5354E-02	6.7648E-03	1.4945E-01	-1.8988E-00	4.5175E-02	1.4782E-02	6.6779E-02	4.5175E-02	6.6779E-00
46	7.0595E-00	4.9837E-01	9.8917E-02	6.9591E-03	1.5058E-01	-1.8912E-00	4.6187E-02	1.4349E-02	6.6274E-02	4.6187E-02	6.6274E-00
47	7.0713E-00	5.0033E-01	1.0185E-01	1.0207E-03	1.5207E-01	-1.8834E-00	4.7356E-02	1.3886E-02	6.5760E-02	4.7356E-02	6.5760E-00
48	7.0831E-00	5.1172E-01	1.0555E-01	1.0447E-03	1.5329E-01	-1.8754E-00	4.8583E-02	1.3428E-02	6.5236E-02	4.8583E-02	6.5236E-00
49	7.0942E-00	5.2337E-01	1.0755E-01	1.0556E-03	1.5555E-01	-1.8672E-00	4.9955E-02	1.2952E-02	6.4702E-02	4.9955E-02	6.4702E-00

TABLE III (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1184E-00	5.0504E-01	1.11361E-01	7.9934E-03	1.5587E-01	-1.8587E-00	5.1283E-02	1.2510E-02	6.4156E-00
51	7.1184E-00	5.0672E-01	1.11952E-01	8.3935E-03	1.5724E-01	-1.8600E-00	5.3379E-02	1.1914E-02	6.3596E-00
52	7.1302E-00	5.0839E-01	1.12529E-01	8.7851E-03	1.5868E-01	-1.8408E-00	5.5362E-02	1.1383E-02	6.3018E-00
53	7.1420E-00	5.1003E-01	1.13238E-01	9.2677E-03	1.6020E-01	-1.8313E-00	5.7850E-02	1.0790E-02	6.2421E-00
54	7.1537E-00	5.1176E-01	1.14107E-01	9.9551E-03	1.6181E-01	-1.8213E-00	6.0905E-02	1.0147E-02	6.1800E-00
55	7.1655E-00	5.1345E-01	1.15216E-01	1.0618E-02	1.6354E-01	-1.8107E-00	6.4924E-02	9.4184E-01	6.1148E-00
56	7.1773E-00	5.1513E-01	1.16738E-01	1.1542E-02	1.6542E-01	-1.7993E-00	7.0488E-02	8.5762E-01	6.0452E-00
57	7.1891E-00	5.1693E-01	1.1971E-01	1.3264E-02	1.6653E-01	-1.7866E-00	7.9173E-02	7.5394E-01	5.9692E-00
58	7.2008E-00	5.1862E-01	2.2317E-01	1.5498E-02	1.6997E-01	-1.7722E-00	9.1171E-02	6.4533E-01	5.8836E-00
59	7.2126E-00	5.2022E-01	2.8403E-01	1.9690E-02	1.7295E-01	-1.7547E-00	1.1385E-01	5.0787E-01	5.7820E-00

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TABLE IV
EXPERIMENTAL DATA FOR SAMPLE 2 AT ROTOR SPEED 17,250 RPM
(See Figure 3a)

THE CONCENTRATION FOR THIS RUN = 0.6737E-01
DIFFERENCE B/W SQS CF B/W AND MENISCUS = 0.12556299E 02
CONC. AT MENISCUS = 0.2446E-01

Identification Number is Sample 2 17,250 RPM

I	R	X	CR	CX	C	LN(C)	Cx/C	1/CX	1/C
1	6.2624E 00	3.92218E 01	9.9452E-04	7.9404E-05	2.4463E-02	-3.7106E 00	3.2459E-03	1.2594E 04	4.0879E 01
2	6.2804E 00	3.9338E 01	2.9836E-03	2.3754E-04	2.4498E-02	-3.7092E 00	4.6966E-03	4.2997E 03	4.0820E 01
3	6.2974E 00	3.9366E 01	4.9726E-03	3.5480E-04	2.4568E-02	-3.7063E 00	1.6070E-02	2.2240E-02	4.0704E 01
4	6.3124E 00	3.9882E 01	5.9673E-03	5.4618E-04	2.4673E-02	-3.7021E 00	2.8481E-02	1.8413E 03	4.0531E 01
5	6.3324E 00	4.0105E 01	8.9507E-03	7.0669E-04	2.4813E-02	-3.6964E 00	2.8481E-02	1.4505E 03	4.0302E 01
6	6.3504E 00	4.0328E 01	1.0940E-02	8.6134E-04	2.4988E-02	-3.6894E 00	3.4471E-02	1.1610E 03	4.0020E 01
7	6.3688E 00	4.0552E 01	1.2929E-02	1.0151E-03	2.5198E-02	-3.6810E 00	4.0287E-02	9.8090E 02	3.0686E 01
8	6.3856E 00	4.0776E 01	1.4918E-02	1.1681E-03	2.5443E-02	-3.6713E 00	4.5910E-02	8.5011E 02	3.9304E 01
9	6.4031E 00	4.1001E 01	1.6907E-02	1.3202E-03	2.5723E-02	-3.6604E 00	5.1323E-02	7.5147E 02	3.0876E 01
10	6.4208E 00	4.1227E 01	1.9890E-02	1.5489E-03	2.6047E-02	-3.6479E 00	5.9466E-02	6.4562E 02	3.8392E 01
11	6.4388E 00	4.1454E 01	2.1875E-02	1.6993E-03	2.6414E-02	-3.6338E 00	6.8236E-02	5.8945E 02	3.7858E 01
12	6.4566E 00	4.1681E 01	2.3668E-02	1.8485E-03	2.6817E-02	-3.6187E 00	6.8931E-02	5.0977E 02	3.7290E 01
13	6.4734E 00	4.1908E 01	2.5858E-02	1.9971E-03	2.7255E-02	-3.6025E 00	7.3277E-02	5.0072E 02	3.6691E 01
14	6.4912E 00	4.2136E 01	2.7847E-02	2.1449E-03	2.7727E-02	-3.5853E 00	7.7358E-02	4.6622E 02	3.6065E 01
15	6.5088E 00	4.2566E 01	2.9836E-02	2.2911E-03	2.8235E-02	-3.5672E 00	8.1113E-02	4.3311E 02	3.5417E 01
16	6.5265E 00	4.2959E 01	3.1825E-02	2.4381E-03	2.8778E-02	-3.5482E 00	8.4728E-02	4.1015E 02	3.7749E 01
17	6.5441E 00	4.2825E 01	3.3814E-02	2.5835E-03	2.9356E-02	-3.5283E 00	8.8009E-02	3.8077E 02	3.4065E 01
18	6.5617E 00	4.3055E 01	3.5803E-02	2.7282E-03	2.9968E-02	-3.5076E 00	9.0355E-02	3.0935E 02	3.3369E 01
19	6.5794E 00	4.3752E-02	2.7752E-02	2.8672E-03	3.0616E-02	-3.4862E 00	9.3808E-02	3.4819E 02	3.2663E 01
20	6.5966E 00	4.3519E 01	3.9781E-02	3.0151E-03	3.1299E-02	-3.4662E 00	9.6333E-02	3.3166E 02	3.1950E 01
21	6.6145E 00	4.3751E 01	4.2764E-02	3.2326E-03	3.2025E-02	-3.4412E 00	1.0099E-01	3.0355E 02	3.1225E 01
22	6.6321E 00	4.3985E 01	4.5748E-02	3.4490E-03	3.2804E-02	-3.4172E 00	2.8944E 02	3.0484E 01	
23	6.6491E 00	4.4218E 01	4.9726E-02	3.7390E-03	3.3645E-02	-3.3919E 00	1.1113E 01	2.67422E 01	
24	6.6677E 00	4.4453E 01	5.4699E-02	4.1020E-03	3.4564E-02	-3.3649E 00	1.1868E-01	2.4378E 02	2.8932E 01
25	6.6845E 00	4.4688E 01	6.1660E-02	4.6119E-03	3.5598E-02	-3.3357E 00	1.2959E-01	2.8099E 02	2.8099E 01
26	6.7022E 00	4.4924E 01	6.8622E-02	5.1191E-03	4.6735E-02	-3.3040E 00	1.3935E-01	1.9555E 02	2.7222E 01
27	6.7201E 00	4.5160E 01	7.4589E-02	5.5497E-03	3.7995E-02	-3.2703E 00	1.4606E-01	1.8019E 02	2.6319E 01
28	6.7377E 00	4.5397E 01	8.1551E-02	6.0518E-03	3.9364E-02	-3.2348E 00	1.5372E-01	1.6324E 02	2.5400E 01
29	6.7553E 00	4.5634E 01	8.8512E-02	6.5513E-03	4.0866E-02	-3.1975E 00	1.6031E-01	1.6264E 02	2.4470E 01
30	6.7729E 00	4.6057E 01	9.8457E-02	7.0205E-03	4.2512E-02	-3.1580E 00	1.7098E-01	1.3758E 02	2.3523E 01
31	6.7904E 00	4.6111E 01	1.0940E-01	8.0551E-03	4.4341E-02	-3.1158E 00	1.8166E-01	1.2444E 02	2.3552E 01
32	6.8081E 00	4.6351E 01	1.2034E-01	8.8377E-03	4.6335E-02	-3.0713E 00	1.9002E-01	1.1315E 02	2.1569E 01
33	6.8257E 00	4.6591E 01	1.3327E-01	9.7620E-03	4.8595E-02	-3.0242E 00	2.0088E-01	1.0466E 02	2.0577E 01
34	6.8433E 00	4.6813E 01	1.4818E-01	1.0827E-02	5.1072E-02	-2.9745E 00	2.1199E-01	9.2633E 01	1.9580E 01
35	6.8606E 00	4.7072E 01	1.6410E-01	1.1959E-02	5.3821E-02	-2.9221E 00	2.2219E-01	8.3621E 01	1.8580E 01
36	6.8785E 00	4.7314E 01	1.8399E-01	1.3377E-02	5.6884E-02	-2.8667E 00	2.3511E-01	7.4772E 01	1.7579E 01
37	6.8961E 00	4.7557E 01	2.0288E-01	1.4710E-02	6.0288E-02	-2.8086E 00	2.4399E-01	6.7822E 01	1.6597E 01
38	6.9137E 00	4.7800E 01	2.2675E-01	1.6399E-02	6.4071E-02	-2.7478E 00	2.5594E-01	6.0811E 01	1.5608E 01
39	6.9311E 00	4.8044E 01	2.5460E-01	1.8366E-02	6.8307E-02	-2.6837E 00	2.6887E-01	5.4450E 01	1.4640E 01
40	6.9499E 00	4.8288E 01	2.7946E-01	2.0100E-02	7.3008E-02	-2.6172E 00	2.7525E-01	4.9731E 01	1.3697E 01
41	6.9666E 00	4.8533E 01	3.1228E-01	2.2413E-02	7.8216E-02	-2.5483E 00	2.8655E-01	4.4617E 01	1.2785E 01
42	6.9842E 00	4.8779E 01	3.5305E-01	2.5275E-02	8.0722E-02	-2.4761E 00	3.0064E-01	3.9544E 01	1.1895E 01
43	7.0018E 00	4.9025E 01	3.9880E-01	2.8479E-02	9.0689E-02	-2.4003E 00	3.1403E-01	3.5141E 01	1.1027E 01
44	7.0194E 00	4.9222E 01	4.5350E-01	3.2304E-02	9.1911E-02	-2.3208E 00	3.2899E-01	3.0562E 01	1.0184E 01
45	7.0370E 00	4.9519E 01	5.1616E-01	3.6675E-02	1.0672E-01	-2.2373E 00	3.4366E-01	2.7667E 01	9.3699E 00
46	7.0544E 00	4.9767E 01	5.9971E-01	4.2504E-02	1.1655E-01	-2.1495E 00	3.6470E-01	2.3521E 01	8.5803E 00
47	7.0722E 00	5.0016E 01	6.9716E-01	4.9289E-02	1.2796E-01	-2.0560E 00	3.8519E-01	2.8150E 01	7.8150E 00
48	7.0892E 00	5.0265E 01	8.0059E-01	5.6461E-02	1.4114E-01	-1.9580E 00	4.0003E-01	1.7711E 01	7.0851E 00
49	7.1074E 00	5.0515E 01	9.6270E-01	6.7725E-02	1.5666E-01	-1.8537E 00	4.3230E-01	1.4766E 01	6.3832E 00

TABLE IV (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1250E 00	5.0768E 01	1.1517E 00	8.0818E-02	1.7527E-01	-1.7414E 00	4.6111E-01	1.2373E 01	5.7055E 00
51	7.1426E 00	5.1017E 01	1.4649E 00	1.0255E-01	1.9830E-01	-1.6180E 00	5.1715E-01	9.7515E 00	5.0430E 00
52	7.1602E 00	5.1269E 01	1.7931E 00	1.2521E-01	2.2697E-01	-1.4829E 00	5.5168E-01	7.9863E 00	4.4059E 00
53	7.1778E 00	5.1521E 01	2.1114E 00	1.4708E-01	2.6133E-01	-1.3420E 00	5.6279E-01	6.7992E 00	3.8265E 00
54	7.1954E 00	5.1774E 01	2.4336E 00	1.6911E-01	3.0134E-01	-1.1995E 00	5.6119E-01	5.9134E 00	3.3186E 00

TABLE V

EXPERIMENTAL DATA FOR SAMPLE 2 AT ROTOR SPEED 10,589 RPM
(See Figure 4)

THE CONCENTRATION FOR THIS RUN = 0.6737×10^{-1}
DIFFERENCE B/TWN SQS OF RTN AND MENISCUS = $0.12693140 \times 10^{-1}$
CNC. AT MENISCUS = 0.3544×10^{-1}

Identification Number is Sample 2 10,589 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.2645E-00	3.9244E-00	1.7955E-002	1.4331E-003	3.5236E-002	-3.3457E-00	4.0671E-002	6.9780E-002	2.8380E-001
2	6.2881E-00	3.9540E-00	1.9172E-002	1.5245E-003	3.5677E-002	-3.3334E-00	4.2735E-002	6.5596E-002	2.8032E-001
3	6.3116E-00	3.9836E-00	2.0592E-002	1.6313E-003	3.6141E-002	-3.3203E-00	4.5137E-002	6.1301E-002	2.7669E-001
4	6.2352E-00	4.0134E-00	2.2114E-002	1.7453E-003	3.6664E-002	-3.3065E-00	4.7629E-002	5.7296E-002	2.7289E-001
5	6.3587E-00	4.0433E-00	2.3737E-002	1.8665E-003	3.7184E-002	-3.2919E-00	5.0195E-002	5.3577E-002	2.6893E-001
6	6.3823E-00	4.0733E-00	2.5553E-002	2.0226E-003	3.7766E-002	-3.2776E-00	5.3029E-002	4.9934E-002	2.6480E-001
7	6.4258E-00	4.1035E-00	2.7479E-002	2.1457E-003	3.8390E-002	-3.2600E-00	5.5893E-002	4.6604E-002	2.6049E-001
8	6.4294E-00	4.1317E-00	2.9620E-002	2.3035E-003	3.9062E-002	-3.2426E-00	4.8970E-002	4.3412E-002	2.5600E-001
9	6.4529E-00	4.1641E-00	3.1954E-002	2.4759E-003	3.9788E-002	-3.2224E-00	6.2228E-002	4.0389E-002	2.5133E-001
10	6.4765E-00	4.1945E-00	3.4490E-002	2.6627E-003	4.0570E-002	-3.2047E-00	6.5631E-002	3.7556E-002	2.44649E-001
11	6.5001E-00	4.2251E-00	3.7127E-002	2.8559E-003	4.1414E-002	-3.1841E-00	6.8960E-002	3.5015E-002	2.4147E-001
12	6.5236E-00	4.2558E-00	3.9676E-002	3.0633E-003	4.2322E-002	-3.1625E-00	7.2381E-002	3.2645E-002	2.3629E-001
13	6.5472E-00	4.2865E-00	4.2115E-002	3.2847E-003	4.3299E-002	-3.1396E-00	7.5860E-002	3.0444E-002	2.3095E-001
14	6.5707E-00	4.3174E-00	4.4657E-002	3.5199E-003	4.4350E-002	-3.1156E-00	7.9366E-002	2.8410E-002	2.2548E-001
15	6.5243E-00	4.3489E-00	4.9765E-002	3.7688E-003	4.5480E-002	-3.0905E-00	8.2867E-002	2.6533E-002	2.1988E-001
16	6.6178E-00	4.3798E-00	5.3213E-002	4.3213E-003	4.6575E-002	-3.0666E-00	7.1000E-002	3.6298E-002	2.1471E-001
17	6.6414E-00	4.4107E-00	5.7314E-002	4.3149E-003	4.7759E-002	-3.0416E-00	9.0348E-002	2.3176E-002	2.0939E-001
18	6.6655E-00	4.4422E-00	6.1379E-002	4.6421E-003	4.9162E-002	-3.0126E-00	9.4423E-002	2.1542E-002	2.0341E-001
19	6.6895E-00	4.4736E-00	6.6749E-002	4.9897E-003	4.0677E-002	-2.9823E-00	9.8461E-002	1.9733E-002	1.9333E-001
20	6.7131E-00	4.5052E-00	7.2225E-002	5.3803E-003	5.2314E-002	-2.9505E-00	1.0285E-001	1.8586E-002	1.9115E-001
21	6.7354E-00	4.5369E-00	7.8312E-002	5.8132E-003	5.4087E-002	-2.9172E-00	1.0748E-001	1.7202E-002	1.8489E-001
22	6.7592E-00	4.5686E-00	8.4395E-002	6.2907E-003	5.6009E-002	-2.8822E-00	1.1214E-001	1.5922E-002	1.7854E-001
23	6.7927E-00	4.6005E-00	9.2209E-002	6.7973E-003	5.8093E-002	-2.8457E-00	1.1700E-001	1.4712E-002	1.7213E-001
24	6.8263E-00	4.6328E-00	1.0032E-001	7.3700E-003	6.0362E-002	-2.8074E-00	1.2210E-001	1.3569E-002	1.6567E-001
25	6.8508E-00	4.6644E-00	1.0391E-001	7.9976E-003	6.2829E-002	-2.7673E-00	1.2718E-001	1.2515E-002	1.5916E-001
26	6.8834E-00	4.6959E-00	1.1968E-001	8.6588E-003	6.5513E-002	-2.7255E-00	1.3217E-001	1.1549E-002	1.5264E-001
27	6.9177E-00	4.7294E-00	1.2913E-001	9.2920E-003	6.8431E-002	-2.6819E-00	1.3720E-001	1.0651E-002	1.4613E-001
28	6.9515E-00	4.7617E-00	1.4260E-001	1.0187E-002	7.1609E-002	-2.6336E-00	1.4227E-001	9.8161E-002	1.3965E-001
29	6.9941E-00	4.7943E-00	1.5379E-001	1.1105E-002	7.5075E-002	-2.5893E-00	1.4792E-001	9.0050E-001	1.3326E-001
30	7.0363E-00	4.8269E-00	1.6769E-001	1.2767E-002	7.8866E-002	-2.5401E-00	1.5302E-001	8.2867E-001	1.2681E-001
31	7.0712E-00	4.8597E-00	1.8230E-001	1.3118E-002	8.299CE-002	-2.4890E-00	1.5807E-001	7.6231E-001	1.2050E-001
32	7.1034E-00	4.8926E-00	1.9963E-001	1.4270E-002	8.7495E-002	-2.4362E-00	1.6310E-001	7.0076E-001	1.1429E-001
33	7.1319E-00	4.9256E-00	2.1779E-001	1.5465E-002	9.2405E-002	-2.3816E-00	1.6737E-001	6.4660E-001	1.0822E-001
34	7.1641RF	4.9589E-00	2.3737E-001	1.6454E-002	9.7759E-002	-2.3253E-00	1.7241E-001	5.9332E-001	1.0230E-001
35	7.19654E-00	4.99079E-00	2.6070E-001	1.94449E-002	1.0362E-002	-2.2670E-00	1.7805E-001	5.4203E-001	9.6506E-001
36	7.22997E-00	5.02753E-00	2.8798E-001	2.1248E-002	1.1070E-002	-2.2066E-00	1.395E-001	4.9387E-001	9.0850E-001
37	7.26125E-00	5.05998E-00	3.1751E-001	2.2320E-002	1.1719E-002	-2.1439E-00	1.9046E-001	4.4802E-001	8.5330E-001
38	7.291361E-00	5.09245E-00	3.5701E-001	2.319E-002	1.2514E-001	-2.0784E-00	1.9993E-001	3.9970E-001	7.9913E-001
39	7.321596E-00	5.12569E-00	4.12983E-001	2.8691E-002	1.3418E-001	-2.0366E-00	2.1382E-001	3.4854E-001	7.4527E-001
40	7.351927E-00	5.15915E-00	4.97756E-001	3.45990E-002	1.4448E-001	-1.9319E-00	2.38882E-001	2.8903E-001	6.9027E-001
41	7.37167E-00	5.1937E-00	7.2220E-001	4.9969E-002	1.5920E-001	-1.8376E-00	3.1387E-001	2.0012E-001	6.2813E-001

TABLE VI

EXPERIMENTAL DATA FOR SAMPLE 2 AT ROTOR SPEED 7,447 RPM
(See Figure 3b)

THE CONCENTRATION FOR THIS RUN = 0.6737×10^{-3}
DIFFERENCE B/TW SGS OF STM AND MENISCUS = $0.12556299 \times 10^{-3}$
CONC. AT MENISCUS = 0.4797×10^{-3}

Identification Number is Sample 2 7,447 RPM

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.2624E 00	3.9218E 01	2.0985E-02	1.66675E-C3	4.7967E-02	-3.0373E 00	3.4763E-02	5.9971E 02	2.0048E 01
2	6.2802E 00	3.9438E 01	2.1879E-02	1.7422E-C3	4.8343E-02	-3.0294E 00	3.6034E-02	5.7406E 02	2.0686E 01
3	6.2976E 00	3.9660E 01	2.1879E-02	1.7371E-C3	4.8728E-02	-3.0215E 00	3.5649E-02	5.7566E 02	2.0222E 01
4	6.3152E 00	3.9882E 01	2.2874E-02	1.8110E-C3	4.9122E-02	-3.0134E 00	3.6868E-02	5.5217E 02	2.0357E 01
5	6.3328E 00	4.0105E 01	2.3868E-02	1.8845E 03	4.9533E-02	-3.0051E 00	3.0455E-02	5.3064E 02	2.0188E 01
6	6.3504E 00	4.0238E 01	2.4863E-02	1.9218E-C3	4.9962E-02	-2.9965E 00	3.1811E-02	5.1083E 02	2.0015E 01
7	6.3680E 00	4.0552E 01	2.5858E-02	2.0303E-C3	5.0409E-02	-2.9816E 00	4.0276E-02	4.9255E 02	1.9938E 01
8	6.3856E 00	4.0776E 01	2.6852E-02	2.0325E-C3	5.0873E-02	-2.9784E 00	4.1329E-02	4.7562E 02	1.9677E 01
9	6.4022E 00	4.1001E 01	2.7847E-02	2.1744E-03	5.1354E-02	-2.9690E 00	4.2341E-02	4.5989E 02	1.9473E 01
10	6.4208E 00	4.1227E 01	2.8841E-02	2.1590E-03	5.1853E-02	-2.9533E 00	4.3313E-02	4.4526E 02	1.9255E 01
11	6.4384E 00	4.1454E 01	2.9839E-02	2.3170E-03	5.2370E-02	-2.9494E 00	4.4243E-02	4.3159E 02	1.9095E 01
12	6.4560E 00	4.1681E 01	3.0839E-02	2.3877E-C3	5.2904E-02	-2.9333E 00	4.5133E-02	4.1881E 02	1.8902E 01
13	6.4736E 00	4.1928E 01	3.1825E-02	2.4580E-C3	5.3455E-02	-2.9289E 00	4.5983E-02	4.0683E 02	1.8707E 01
14	6.4913E 00	4.2136E 01	2.819E-02	2.5452E-C3	5.4024E-02	-2.9183E 00	4.6793E-02	3.8510E 02	1.8510E 01
15	6.5089E 00	4.2356E 01	3.3814E-02	2.5575E-C3	5.4611E-02	-2.9075E 00	4.7564E-02	3.8498E 02	1.8311E 01
16	6.5265E 00	4.2595E 01	3.4808E-02	2.6667E-C3	5.5215E-02	-2.8865E 00	4.8297E-02	3.7500E 02	1.8111E 01
17	6.5441E 00	4.2825E 01	3.5803E-02	2.7355E-C3	5.5836E-02	-2.8833E 00	4.8992E-02	3.6566E 02	1.7910E 01
18	6.5617E 00	4.3055E 01	3.6040E-02	2.8040E-C3	5.6475E-02	-2.8740E 00	4.9649E-02	3.5664E 02	1.7710E 01
19	6.5793E 00	4.3287E 01	3.7779E-02	2.8720E-C3	5.7132E-02	-2.8624E 00	5.0270E-02	3.4819E 02	1.7503E 01
20	6.5969E 00	4.3519E 01	3.8786E-02	2.9397E-03	5.7805E-02	-2.8507E 00	5.0856E-02	3.4017E 02	1.7299E 01
21	6.6145E 00	4.3751E 01	3.9781E-02	3.0711E-03	5.8497E-02	-2.8388E 00	5.1406E-02	3.3253E 02	1.7095E 01
22	6.6321E 00	4.3958E 01	4.0775E-02	3.0741E-03	5.9206E-02	-2.8287E 00	5.1922E-02	3.2530E 02	1.6890E 01
23	6.6497E 00	4.4218E 01	4.1770E-02	3.1407E-03	5.9933E-02	-2.8155E 00	5.2404E-02	3.1840E 02	1.6665E 01
24	6.6673E 00	4.4453E 01	4.3779E-02	3.2816E-03	6.0686E-02	-2.8020E 00	5.4076E-02	3.0473E 02	1.6418E 01
25	6.6849E 00	4.4688E 01	4.4753E-02	3.4347E-03	6.1456E-02	-2.7893E 00	5.4874E-02	2.6702E 02	1.6270E 01
26	6.7025E 00	4.4924E 01	4.5748E-02	3.4128E-03	6.2261E-02	-2.7764E 00	5.4813E-02	2.9302E 02	1.6061E 01
27	6.7201E 00	4.5160E 01	4.6742E-02	3.4778E-03	6.3075E-02	-2.7634E 00	5.5137E-02	2.8754E 02	1.5854E 01
28	6.7377E 00	4.5397E 01	4.8731E-02	3.6163E-03	6.3916E-02	-2.7502E 00	5.6580E-02	2.7652E 02	1.5664E 01
29	6.7553E 00	4.5634E 01	4.9766E-02	3.6802E-03	6.4782E-02	-2.7376E 00	5.6814E-02	2.7137E 02	1.5456E 01
30	6.7729E 00	4.5872E 01	5.1715E-02	3.8178E-03	6.5675E-02	-2.7330E 00	5.8131E-02	2.6193E 02	1.5226E 01
31	6.7905E 00	4.6111E 01	5.3704E-02	3.9543E-03	6.6603E-02	-2.7090E 00	5.9372E-02	2.5289E 02	1.5014E 01
32	6.8081E 00	4.6351E 01	5.4699E-02	4.0172E-03	6.7276E-02	-2.6948E 00	5.9463E-02	2.4893E 02	1.4892E 01
33	6.8257E 00	4.6591E 01	5.6688E-02	4.1525E-03	6.8538E-02	-2.6804E 00	6.0587E-02	2.4082E 02	1.4691E 01
34	6.8433E 00	4.6831E 01	5.8677E-02	4.2871E-03	6.9553E-02	-2.6657E 00	6.1639E-02	2.3326E 02	1.4318E 01
35	6.8609E 00	4.7072E 01	5.9671E-02	4.3486E-03	7.0595E-02	-2.6508E 00	6.1600E-02	2.2996E 02	1.4165E 01
36	6.8785E 00	4.7314E 01	6.1660E-02	4.4182E-03	7.1663E-02	-2.6338E 00	6.2544E-02	2.2311E 02	1.3934E 01
37	6.8961E 00	4.7557E 01	6.3649E-02	4.6148E-03	7.2766E-02	-2.6205E 00	6.3442E-02	2.1669E 02	1.3743E 01
38	6.9137E 00	4.7800E 01	6.5638E-02	4.7469E-03	7.3904E-02	-2.6050E 00	6.4232E-02	2.1066E 02	1.3531E 01
39	6.9314E 00	4.8044E 01	6.8622E-02	4.9501E-03	7.5085E-02	-2.5893E 00	6.5926E-02	2.0202E 02	1.2228E 01
40	6.9490E 00	4.8288E 01	7.1605E-02	5.1522E-03	7.6320E-02	-2.5728E 00	6.7509E-02	1.9409E 02	1.2030E 01
41	6.9666E 00	4.8533E 01	7.4589E-02	5.3134E-03	7.7606E-02	-2.5561E 00	6.8981E-02	1.8680E 02	1.2886E 01
42	6.9842E 00	4.8877E 01	7.7575E-02	5.5535E-03	7.8946E-02	-2.5390E 00	7.0345E-02	1.8007E 02	1.2667E 01
43	7.0018E 00	4.9025E 01	8.05556E-02	5.7553E-03	8.0337E-02	-2.5215E 00	7.1605E-02	1.7384E 02	1.2448E 01
44	7.0194E 00	4.9272E 01	8.3545E-02	5.9507E-03	8.1782E-02	-2.5037E 00	7.2773E-02	1.6845E 02	1.2228E 01
45	7.0370E 00	4.9519E 01	8.6523E-02	6.1478E-03	8.3279E-02	-2.4836E 00	7.3822E-02	1.6265E 02	1.2008E 01
46	7.0546E 00	4.9767E 01	8.9507E-02	6.3439E-03	8.4828E-02	-2.4671E 00	7.4785E-02	1.5763E 02	1.1789E 01
47	7.0722E 00	5.0016E 01	9.2490E-02	6.5903E-03	8.6430E-02	-2.4484E 00	7.5297E-02	1.5293E 02	1.1570E 01
48	7.0898E 00	5.0256E 01	9.5457E-02	6.9436E-03	8.8111E-02	-2.4292E 00	7.8806E-02	1.4402E 02	1.1349E 01
49	7.1074E 00	5.0515E 01	1.0741E-01	7.5561E-C3	8.9922E-02	-2.4088E 00	8.4029E-02	1.3234E 02	1.1121E 01

TABLE VI (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1250E 20	5.02766E C1	1.1730E-01	8.2353E-C3	9.1901E-02	-2.3870E 00	8.9611E-02	1.2143E C2	1.0881E 01
51	7.1426E 20	5.1017E C1	1.2730E-01	8.9112F-C3	9.4054E-02	-2.3639E 00	9.4746E-02	1.1222E C2	1.0632E 01
52	7.1502E 20	5.1269E C1	1.4520E-01	1.0139E-C2	9.6452E-02	-2.3387E 00	1.0512E-01	9.8625E C1	1.0368E 01
53	7.1778E 20	5.1521E C1	1.7867E-C1	1.2401E-C2	9.9297E-02	-2.3096E 00	1.2488E-01	8.0641E 01	1.0071E 01
54	7.1954E 20	5.1774E C1	2.5559E-01	1.7761E-C2	1.0311E-01	-2.2719E 00	1.7225E-01	5.6304E 01	9.6981E 00

TABLE VII

EXPERIMENTAL DATA FOR SAMPLE 3 AT ROTOR SPEED 10,589 RPM
(See Figure 5)

THE CONCENTRATION FOR THIS RUN = 0.1146×10^{-6}
DIFFERENCE BTWN SQS OF BTW AND MENISCUS = $0.12987963 \times 10^{-6}$
CONC. AT MENISCUS = 0.6796×10^{-6}

Identification Number Is Sample 3 10,589 RPM

I	R	X	CR	CX	C	LNC(C)	CX/C	I/CX	I/C
1	6.2486E-00	3.9045E-01	4.9353E-02	3.9491E-C3	6.7960E-02	-2.6888E-00	5.8109E-02	2.5322E-02	1.4715E-01
2	6.2778E-00	3.9411E-01	5.0205E-02	4.0018E-03	6.9418E-02	-2.6676E-00	5.7709E-02	2.4932E-02	1.4406E-01
3	6.3771E-00	3.9779E-01	5.2374E-02	4.1520E-03	7.0919E-02	-2.6622E-00	5.8546E-02	2.4085E-02	1.401E-01
4	6.3363E-00	4.0149E-01	5.3382E-02	4.2124E-03	7.2465E-02	-2.6246E-00	5.8129E-02	2.3740E-02	1.3800E-01
5	6.6655E-00	4.0520E-01	5.5396E-02	4.3512E-03	7.5704E-02	-2.5029E-00	5.8794E-02	2.2977E-02	1.3503E-01
6	6.3948E-00	4.0893E-01	5.7410E-02	4.4888E-03	7.5704E-02	-2.5309E-00	5.9294E-02	2.2277E-02	1.3209E-01
7	6.6244E-00	4.1268E-01	5.8418E-02	4.5468E-03	7.7398E-02	-2.5188E-00	5.8746E-02	2.1993E-02	1.2920E-01
8	6.4523E-00	4.1644E-01	6.0432E-02	4.6823E-03	7.9135E-02	-2.5136E-00	5.9169E-02	2.1357E-02	1.2637E-01
9	6.4125E-00	4.2023E-01	6.1434E-02	4.7389E-03	8.0916E-02	-2.5143E-00	5.8656E-02	2.1102E-02	1.2358E-01
10	6.5117E-00	4.2403E-01	6.3424E-02	4.8723E-03	8.2742E-02	-2.4920E-00	5.8885E-02	2.0524E-02	1.2086E-01
11	6.5411E-00	4.2794E-01	6.7494E-02	5.1584E-03	8.4656E-02	-2.4652E-00	6.0934E-02	1.9386E-02	1.1813E-01
12	6.6702E-00	4.3167E-01	7.2518E-02	5.5187E-03	8.6702E-02	-2.4453E-00	6.3652E-02	1.8120E-02	1.1534E-01
13	6.5504E-00	4.3553E-01	7.7554E-02	5.8758E-03	8.8896E-02	-2.403E-00	6.6098E-02	1.7019E-02	1.1249E-01
14	6.6877E-00	4.3839E-01	8.2592E-02	6.2298E-03	9.1237E-02	-2.3943E-00	6.8282E-02	1.6052E-02	1.0961E-01
15	6.6579E-00	4.4329E-01	9.0648E-02	6.9075E-03	9.3769E-02	-2.3669E-00	7.2599E-02	1.4690E-02	1.0665E-01
16	6.6671E-00	4.4718E-01	9.7694E-02	7.3049E-03	9.6522E-02	-2.3380E-00	7.5682E-02	1.3689E-02	1.0360E-01
17	6.7164E-00	4.5110E-01	1.0374E-01	7.7230E-03	9.9466E-02	-2.3019E-00	7.7645E-02	1.2948E-02	1.0054E-01
18	6.6456E-00	4.5533E-01	1.1717E-01	8.2122E-03	1.0260E-01	-2.2169E-00	8.0039E-02	1.2177E-02	9.7464E-01
19	6.7748E-00	4.5893E-01	1.1988E-01	8.8457E-03	1.0597E-01	-2.2446E-00	8.3471E-02	1.1305E-02	9.4363E-00
20	6.8041E-00	4.6296E-01	1.2392E-01	9.4738E-03	1.0903E-01	-2.208E-00	8.6432E-02	1.0555E-02	9.1233E-00
21	6.8337E-00	4.6664E-01	1.3799E-01	1.0397E-02	1.1351E-01	-2.1759E-00	8.8948E-02	9.9043E-02	8.8697E-00
22	6.6526E-00	4.7095E-01	1.4906E-01	1.3787E-02	1.1769E-01	-2.1397E-00	9.1658E-02	9.2701E-01	8.4967E-00
23	6.8918E-00	4.7497E-01	1.5813E-01	1.1472E-02	1.2217E-01	-2.1024E-00	9.3907E-02	8.7169E-01	8.1855E-00
24	6.9214E-00	4.7911E-01	1.7202E-01	1.2297E-02	1.2697E-01	-2.0638E-00	9.6852E-02	8.1320E-01	7.8760E-00
25	6.6583E-00	4.8316E-01	1.8313E-01	1.3187E-02	1.3213E-01	-2.0239E-00	9.9802E-02	7.5831E-01	7.568CE-00
26	6.0795E-00	4.8713E-01	2.0133E-01	1.4359E-02	1.3774E-01	-1.924E-00	1.0424E-01	6.9644E-01	7.2598E-00
27	7.0397E-00	4.9122E-01	2.2158E-01	1.5908E-02	1.4391E-01	-1.9386E-00	1.0984E-01	6.3220E-01	6.9487E-00
28	7.0397E-00	4.9533E-01	2.4475E-01	1.7388E-02	1.5073E-01	-1.8923E-00	1.1536E-01	5.7512E-01	6.6344E-00
29	7.5972E-00	4.9945E-01	2.7494E-01	1.9454E-02	1.5832E-01	-1.8431E-00	1.2287E-01	5.1404E-01	6.3161E-00
30	7.2064E-00	5.0362E-01	3.1425E-01	2.2141E-02	1.6694E-01	-1.7901E-00	1.3263E-01	4.5165E-01	5.9903E-00
31	7.1257E-00	5.0775E-01	3.6658E-01	2.5725F-02	1.7689E-01	-1.7322E-00	1.4543E-01	3.8872E-01	5.5333E-00
32	7.1549E-00	5.1193E-01	4.6925E-01	3.1321E-02	1.9882E-01	-1.6671E-00	1.6590E-01	3.1927E-01	5.2967E-00
33	7.1942E-00	5.1612E-01	6.7482E-01	2.0521E-02	2.0521E-01	-1.5337E-00	2.2887E-01	2.1292E-01	4.8731E-00
34	7.2134E-00	5.2033E-01	1.0012E-00	2.2978E-01	1.4706E-01	-1.4706E-00	3.0383E-01	4.3519E-01	4.3519E-00

TABLE VIII

EXPERIMENTAL DATA FOR SAMPLE 3 AT ROTOR SPEED 8,766 RPM
(See Figure 6a)

THE CONCENTRATION FOR THIS RUN = $0.11146E-90$
DIFFERENCE BTWN SQS OF BT4 AND MENISCUS = $0.12829269E-02$
CONE. AT MFNTSCUS = $0.8063E-01$

I	q	x	CR	CX	C	LN(C)	CX/C	CX/CX	1/CX	1/C
1	6.2464E-20	3.9523E-01	4.1592E-02	3.3289E-03	8.0627E-02	-2.5179E-00	4.1288E-02	3.0040E-02	1.2403E-01	1.2403E-01
2	6.2645E-00	3.9244E-01	4.2302E-02	3.3762E-03	8.1368E-02	-2.5088E-00	4.14493E-02	2.9619E-02	1.2290E-01	1.2290E-01
3	6.2821E-10	3.9555E-01	4.3213E-02	3.4344E-03	8.2123E-02	-2.4995E-00	4.1881E-02	2.9075E-02	1.2177E-01	1.2177E-01
4	6.2598E-00	3.9697E-01	4.4126E-02	3.5022E-03	8.2895E-02	-2.4902E-00	4.2249E-02	2.5533E-02	1.2063E-01	1.2063E-01
5	6.3175E-01	3.9910E-01	4.5039E-02	3.5647E-02	8.3683E-02	-2.4807E-00	4.2597E-02	2.8053E-02	1.1950E-01	1.1950E-01
6	6.3351E-00	4.0134E-01	4.6054E-02	3.6348E-02	8.4487E-02	-2.4712E-00	4.3022E-02	2.7512E-02	1.1836E-01	1.1836E-01
7	6.3522E-00	4.0158E-01	4.7054E-02	3.7045E-02	8.5310E-02	-2.4615E-00	4.3424E-02	2.6994E-02	1.1722E-01	1.1722E-01
8	6.3770E-10	4.0583E-01	4.8083E-02	3.8508E-02	8.6150E-02	-2.4517E-00	4.3806E-02	2.6498E-02	1.1608E-01	1.1608E-01
9	6.3891E-00	4.0809E-01	4.9193E-02	3.9018E-02	8.7010E-02	-2.4417E-00	4.4257E-02	2.5969E-02	1.1493E-01	1.1493E-01
10	6.4058E-20	4.1034E-01	5.0314E-02	3.9521E-02	8.7889E-02	-2.4317E-00	4.4684E-02	2.5463E-02	1.1378E-01	1.1378E-01
11	6.4235E-01	4.1261E-01	5.1532E-02	4.0112E-02	8.8788E-02	-2.4215E-00	4.5177E-02	2.4930E-02	1.1263E-01	1.1263E-01
12	6.4411E-20	4.1498E-01	5.2419E-02	4.0947E-02	8.9709E-02	-2.4112E-00	4.5642E-02	2.4422E-02	1.1147E-01	1.1147E-01
13	6.4589E-00	4.1716E-01	5.3966E-02	4.1777E-02	9.0652E-02	-2.4010E-00	4.6084E-02	2.3937E-02	1.1031E-01	1.1031E-01
14	6.4765E-02	4.1945E-01	5.5285E-02	4.2661E-02	9.1617E-02	-2.3901E-00	4.6587E-02	2.3429E-02	1.0915E-01	1.0915E-01
15	6.4941E-20	4.2174E-01	5.6604E-02	4.3580E-02	9.2606E-02	-2.3794E-00	4.7060E-02	2.2946E-02	1.0798E-01	1.0798E-01
16	6.5118E-20	4.2404E-01	5.7934E-02	4.4533E-02	9.3618E-02	-2.3685E-00	4.7590E-02	2.2464E-02	1.0682E-01	1.0682E-01
17	6.5295E-20	4.2634E-01	5.9444E-02	4.5522E-02	9.4656E-02	-2.3575E-00	4.8090E-02	2.1969E-02	1.0565E-01	1.0565E-01
18	6.5471E-00	4.2865E-01	6.0864E-02	4.6481E-02	9.5718E-02	-2.4007E-00	4.8586E-02	2.1514E-02	1.0447E-01	1.0447E-01
19	6.5549E-02	4.3097E-01	6.2388E-02	4.7515E-02	9.6802E-02	-2.3355E-00	4.9082E-02	2.0464E-02	1.0330E-01	1.0330E-01
20	6.5925E-01	4.2239E-01	6.3977E-02	4.8533E-02	9.7923E-02	-2.3236E-00	4.9573E-02	2.0606E-02	1.0212E-01	1.0212E-01
21	6.6521E-00	4.3562E-01	6.5530E-02	4.9643E-02	9.9066E-02	-2.3120E-00	5.0111E-02	2.0144E-02	1.0094E-01	1.0094E-01
22	6.6178E-10	4.3795E-01	6.7153E-02	5.0737E-02	1.0024E-01	2.3002E-00	5.0616E-02	1.9710E-02	9.9762E-00	9.9762E-00
23	6.6355E-20	4.4030E-01	6.8978E-02	5.1301E-02	1.0144E-01	2.2838E-00	5.1165E-02	1.9267E-02	9.8581E-00	9.8581E-00
24	6.6531E-00	4.4264E-01	7.0622E-02	5.2359E-02	1.0267E-01	2.2762E-00	5.1679E-02	1.8847E-02	9.7398E-00	9.7398E-00
25	6.6709E-20	4.4500E-01	7.2428E-02	5.4387E-02	1.0394E-01	2.2640E-00	5.2232E-02	1.8420E-02	9.6214E-00	9.6214E-00
26	6.6849E-00	4.4736E-01	7.4254E-02	5.5509E-02	1.0523E-01	2.2516E-00	5.2750E-02	1.8015E-02	9.5029E-00	9.5029E-00
27	6.7761E-00	4.5727E-01	7.6181E-02	5.6860E-02	1.0656E-01	2.1736E-00	5.3203E-02	1.7606E-02	9.3844E-00	9.3844E-00
28	6.7234E-20	4.5210E-01	7.8210E-02	5.8159E-02	1.0792E-01	2.2226E-00	5.3889E-02	1.7194E-02	9.2658E-00	9.2658E-00
29	6.7415E-00	4.5547E-01	8.0342E-02	5.9581E-02	1.0932E-01	2.2134E-00	5.4505E-02	1.6782E-02	9.1471E-00	9.1471E-00
30	6.7591E-02	4.5686E-01	8.2572E-02	6.1282E-02	1.1076E-01	2.2047E-00	5.5146E-02	1.6371E-02	9.0283E-00	9.0283E-00
31	6.7758E-10	4.5925E-01	8.4710E-02	6.3271E-02	1.1244E-01	2.1871E-00	5.5877E-02	1.5944E-02	8.9092E-00	8.9092E-00
32	6.7944E-00	4.6165E-01	9.7543E-02	6.6422F-02	1.1377E-01	2.1736E-00	5.6626E-02	1.5523E-02	8.7898E-00	8.7898E-00
33	6.8111E-20	4.6405E-01	9.9322E-02	6.8265E-02	1.1534E-01	2.1599E-00	5.7453E-02	1.5091E-02	8.6701E-00	8.6701E-00
34	6.8298E-00	4.6666E-01	9.3122E-02	6.8173E-02	1.1698E-01	2.1459E-00	5.8450E-02	1.4669E-02	8.5500E-00	8.5500E-00
35	6.8475E-00	4.6949E-01	9.6165E-02	7.0219E-02	1.1863E-01	2.1317E-00	5.9192E-02	1.4241E-02	8.4295E-00	8.4295E-00
36	6.8651E-00	4.7130E-01	9.9310E-02	7.2229E-02	1.2036E-01	2.1173E-00	6.0095E-02	1.3826E-02	8.3086E-00	8.3086E-00
37	6.8828E-00	4.7473E-01	1.0275E-01	7.4649E-02	1.2214E-01	2.1026E-00	6.1116E-02	1.3396E-02	8.1872E-00	8.1872E-00
38	6.9015E-00	4.7617E-01	1.0241E-01	7.7174E-02	1.2399E-01	2.0876E-00	6.2155E-02	1.2970E-02	8.0652E-00	8.0652E-00
39	6.9181E-00	4.7861E-01	1.0137E-01	7.9766E-02	1.2590E-01	2.0722E-00	6.3354E-02	1.2537E-02	7.9425E-00	7.9425E-00
40	6.9358E-00	4.8115E-01	1.01463E-01	8.2534E-02	1.2789E-01	2.0566E-00	6.4612E-02	1.2102E-02	7.8191E-00	7.8191E-00
41	6.9535E-02	4.8351E-01	1.01929E-01	8.518CE-02	1.2996E-01	2.0405E-00	6.6005E-02	1.1651E-02	7.6948E-00	7.6948E-00
42	6.9711E-00	4.8597E-01	1.02437E-01	8.9000E-02	1.3211E-01	2.0241E-00	6.7519E-02	1.1211E-02	7.5694E-00	7.5694E-00
43	5.3888E-00	4.8844E-01	1.02994E-01	9.2966E-02	1.3436E-01	2.0273E-00	6.9193E-02	1.0757E-02	7.4428E-00	7.4428E-00
44	7.1745E-01	4.9073E-01	1.03603E-01	9.7775E-02	1.3671E-01	1.9899E-01	7.1010E-02	1.0301E-02	7.3145E-00	7.3145E-00
45	7.2241E-00	4.9239E-01	1.04293E-01	1.0174E-02	1.3917E-01	1.9721E-01	7.3105E-02	9.8289E-02	7.1854E-00	7.1854E-00
46	7.4186E-02	4.9545E-01	1.05497E-01	1.0699E-01	1.4176E-01	1.9536E-01	7.5399E-02	9.3556E-02	7.0540E-00	7.0540E-00
47	7.5595E-00	4.9826E-01	1.05926E-01	1.1280E-02	1.4450E-01	1.9345E-01	7.6062E-02	8.8653E-01	6.9204E-00	6.9204E-00
48	7.6777E-01	5.0186E-01	1.06540E-01	1.1698E-02	1.4740E-01	1.9146E-01	8.1196E-02	8.3553E-01	6.7841E-00	6.7841E-00
49	7.7949E-00	5.0336E-01	1.0361E-01	1.2399E-02	1.5052E-01	1.8937E-01	8.5965E-02	7.7283E-01	6.6436E-00	6.6436E-00

TABLE VIII (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1125E 00	5.0587E 01	2.0095E 01	1.4120E 01	1.5392E 01	-1.8713E 00	9.1735E 02	7.0823E 01	6.4497E 00
51	7.1311E 00	5.0839E 01	2.2114E 01	1.5507E 02	1.5764E 01	-1.8474E 00	9.8369E 02	6.4486E 01	6.3434E 00
52	7.1478E 00	5.1091E 01	2.4356E 01	1.7030E 02	1.6175E 01	-1.8217E 00	1.0529E 01	5.8720E 01	6.1823E 00
53	7.1655E 00	5.1344E 01	2.8423E 01	1.9819E 02	1.6641E 01	-1.7933E 00	1.1910E 01	5.0455E 01	6.0094E 00
54	7.1832E 00	5.1598E 01	3.3475E 01	2.3301E 02	1.7187E 01	-1.7610E 00	1.2557E 01	4.2916E 01	5.8183E 00
55	7.2008E 00	5.1852E 01	4.3619E 01	3.0288E 02	1.7868E 01	-1.7221E 00	1.6951E 01	3.3017E 01	5.5963E 00

TABLE IX

EXPERIMENTAL DATA FOR SAMPLE 3 AT ROTOR SPEED 7,447 RPM
(See Figure 6b)

THE CONCENTRATION FOR THIS RUN = 0.1146E-00
DIFFERENCE BTWN SQS OF BTM AND MENISCUS = 0.12629269E-02
CNC. AT MENISCUS = 0.8673E-01

Identification Number is Sample 3 7,447 RPM

I	Q	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.2468E-00	3.9023E-01	3.8547E-02	3.05654E-03	6.6728E-02	-2.4450E-00	3.5575E-02	3.2411E-02	1.1530E-01
2	6.2645E-00	3.9244E-01	3.8750E-02	3.0928E-03	8.7410E-02	-2.4371E-00	3.2333E-02	1.1440E-01	1.1351E-01
3	6.2221E-00	3.9465E-01	3.9054E-02	3.1384E-03	8.8078E-02	-2.4293E-00	3.2523E-02	3.2171E-02	1.1351E-01
4	6.2998E-00	3.9687E-01	3.9460E-02	3.1319E-03	8.8791E-02	-2.4215E-00	3.5222E-02	3.1930E-02	1.1262E-01
5	6.3115E-00	3.9910E-01	3.9866E-02	3.1522E-03	8.9492E-02	-2.4136E-00	3.5257E-02	3.1694E-02	1.1174E-01
6	6.3351E-00	4.0134E-01	4.0373E-02	3.1864E-03	9.0201E-02	-2.4057E-00	3.5326E-02	3.1383E-02	1.1086E-01
7	6.3528E-00	4.0583E-01	4.0891E-02	3.2175E-03	9.0919E-02	-2.3978E-00	3.5389E-02	3.1080E-02	1.0999E-01
8	6.3715E-00	4.0831E-00	4.1383E-02	3.2484E-03	9.1645E-02	-2.3898E-00	3.5443E-02	3.0784E-02	1.0912E-01
9	6.3881E-00	4.0808E-01	4.1996E-02	3.2870E-03	9.2382E-02	-2.3818E-00	3.5581E-02	3.0422E-02	1.0825E-01
10	6.4058E-00	4.1034E-01	4.2605E-02	3.3255E-03	9.3129E-02	-2.3738E-00	3.5708E-02	3.0171E-02	1.0738E-01
11	6.4225E-00	4.1261E-01	4.3315E-02	3.3716E-03	9.3888E-02	-2.3657E-00	3.5911E-02	2.9659E-02	1.0651E-01
12	6.4411E-00	4.1488E-01	4.4025E-02	3.4115E-03	9.4660E-02	-2.3575E-00	3.6103E-02	2.9261E-02	1.0564E-01
13	6.4588E-00	4.1716E-01	4.4836E-02	3.4710E-03	9.5445E-02	-2.3492E-00	3.6366E-02	2.8810E-02	1.0477E-01
14	6.4765E-00	4.1945E-01	4.5643E-02	3.5244E-03	9.6244E-02	-2.3409E-00	3.6617E-02	2.8376E-02	1.0396E-01
15	6.4941E-00	4.2174E-01	4.6460E-02	3.5710E-03	9.7057E-02	-2.3325E-00	3.6851E-02	2.7956E-02	1.0303E-01
16	6.5118E-00	4.2404E-01	4.7372E-02	3.6314E-03	9.7886E-02	-2.3239E-00	3.7160E-02	2.7492E-02	1.0216E-01
17	6.5295E-00	4.2634E-01	4.8285E-02	3.6975E-03	9.8731E-02	-2.3154E-00	3.7450E-02	2.7045E-02	1.0129E-01
18	6.5471E-00	4.2865E-01	4.9300E-02	3.7650E-03	9.9593E-02	-2.3071E-00	3.7804E-02	2.6565E-02	1.0041E-01
19	6.5648E-00	4.3097E-01	5.0416E-02	3.8339E-03	1.0047E-01	-2.2979E-00	3.8217E-02	2.6043E-02	9.9528E-00
20	6.5825E-00	4.3329E-01	5.1633E-02	3.9220E-03	1.0138E-01	-2.2889E-00	3.8688E-02	2.5497E-02	9.8643E-00
21	6.6021E-00	4.3562E-01	5.2850E-02	4.0370E-03	1.0250E-01	-2.2796E-00	3.9138E-02	2.4977E-02	9.7773E-00
22	6.6178E-00	4.3795E-01	5.4069E-02	4.0505E-03	1.0324E-01	-2.2707E-00	3.9567E-02	2.4480E-02	9.6859E-00
23	6.6355E-00	4.4030E-01	5.5386E-02	4.1135E-03	1.0421E-01	-2.2613E-00	4.0049E-02	2.3981E-02	9.5960E-00
24	6.6531E-00	4.4264E-01	5.6808E-02	4.2691E-03	1.0520E-01	-2.2519E-00	4.0424E-02	2.3448E-02	9.5056E-00
25	6.6709E-00	4.4500E-01	5.8370E-02	4.3633E-03	1.0622E-01	-2.2423E-00	4.1088E-02	2.2913E-02	9.4147E-00
26	6.6885E-00	4.4736E-01	5.9748E-02	4.4665E-03	1.0726E-01	-2.2325E-00	4.1642E-02	2.2389E-02	9.3232E-00
27	6.7061E-00	4.4972E-01	6.1371E-02	4.5575E-03	1.0833E-01	-2.2226E-00	4.2239E-02	2.1854E-02	9.2311E-00
28	6.7238E-00	4.5210E-01	6.3096E-02	4.6692E-03	1.0943E-01	-2.2125E-00	4.2877E-02	2.1313E-02	9.1384E-00
29	6.7415E-00	4.5447E-01	6.4820E-02	4.8076E-03	1.1056E-01	-2.2022E-00	4.3484E-02	2.0801E-02	9.0450E-00
30	6.7591E-00	4.5686E-01	6.6646E-02	4.9301E-03	1.1172E-01	-2.1918E-00	4.4129E-02	2.0284E-02	8.9510E-00
31	6.7768E-00	4.5925E-01	6.8573E-02	5.0594E-03	1.1291E-01	-2.1811E-00	4.4808E-02	1.9765E-02	8.8563E-00
32	6.7945E-00	4.6156E-01	7.0602E-02	5.1665E-03	1.1414E-01	-2.1730E-00	4.5618E-02	1.9247E-02	8.7690E-00
33	6.8121E-00	4.6405E-01	7.2723E-02	5.2384E-03	1.1541E-01	-2.1593E-00	4.6256E-02	1.8732E-02	8.6648E-00
34	6.8298E-00	4.6646E-01	7.4966E-02	5.4880E-03	1.1671E-01	-2.1480E-00	4.7021E-02	1.8222E-02	8.5679E-00
35	6.8475E-00	4.6888E-01	7.7297E-02	5.6644E-03	1.1806E-01	-2.1366E-00	4.7717E-02	1.7771E-02	8.4703E-00
36	6.8651E-00	4.7130E-01	7.9833E-02	5.8144E-03	1.1945E-01	-2.1249E-00	4.8676E-02	1.7197E-02	8.3719E-00
37	6.8828E-00	4.7373E-01	8.2577E-02	5.9984E-03	1.2088E-01	-2.1129E-00	4.9622E-02	1.6671E-02	8.2725E-00
38	6.9005E-00	4.7617E-01	8.5514E-02	6.1962E-03	1.2237E-01	-2.1007E-00	5.0633E-02	1.6139E-02	8.1722E-00
39	6.9181E-00	4.7861E-01	8.8659E-02	6.4077E-03	1.2391E-01	-2.0882E-00	5.1714E-02	1.5606E-02	8.0707E-00
40	6.9358E-00	4.8105E-01	9.2108E-02	6.6400E-03	1.2550E-01	-2.0754E-00	5.2290E-02	1.5060E-02	7.9680E-00
41	6.9535E-00	4.8351E-01	9.5759E-02	6.8837E-03	1.2716E-01	-2.0623E-00	5.4149E-02	1.4523E-02	7.8646E-00
42	6.9711E-00	4.9579E-01	9.9716E-02	7.1520E-03	1.2889E-01	-2.0488E-00	5.5490E-02	1.3982E-02	7.7587E-00
43	6.9888E-00	4.8844E-01	1.0398E-01	7.4487E-03	1.3086E-01	-2.0349E-00	5.6920E-02	1.3443E-02	7.6519E-00
44	7.0065E-00	4.9091E-01	1.0854E-01	7.7457E-03	1.3256E-01	-2.0207E-00	5.8430E-02	1.2910E-02	7.5435E-00
45	7.0241E-00	4.9339E-01	1.1366E-01	8.0973E-03	1.3453E-01	-2.0066E-00	6.0117E-02	1.2365E-02	7.4335E-00
46	7.0418E-00	4.9587E-01	1.1909E-01	8.4660E-03	1.3658E-01	-1.9908E-00	6.1911E-02	1.1866E-02	7.3216E-00
47	7.0595E-00	4.9836E-01	1.2518E-01	8.8659E-03	1.3874E-01	-1.9752E-00	6.3290E-02	1.1279E-02	7.2077E-00
48	7.0771E-00	5.0086E-01	1.3207E-01	9.3311E-03	1.4101E-01	-1.9589E-00	6.6172E-02	1.0717E-02	7.0916E-00
49	7.0948E-00	5.0336E-01	1.4019E-01	9.8798E-03	1.4342E-01	-1.9420E-00	6.8888E-02	1.0122E-02	6.9727E-00

TABLE IX (CONT)

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
50	7.1125E 00	5.0587E 01	1.5013E-01	1.0554E-02	1.4598E-02	1.9243E 00	7.2297E-02	9.4750E 01	6.8502E 00
51	7.1101E 00	5.0839E 01	1.6322E-01	1.1453E-02	1.4875E-02	1.9055E 00	7.6992E-02	8.7316E 01	6.7227E 00
52	7.1478E 00	5.1091E 01	1.8259E-01	1.2773E-02	1.5181E-02	1.8852E 00	8.4138E-02	7.8293E 01	6.5874E 00
53	7.1655E 00	5.1344E 01	2.1322E-01	1.4865E-02	1.5530E-02	1.8624E 00	9.5715E-02	6.7274E 01	6.4391E 00
54	7.1832E 00	5.1598E 01	2.5369E-01	1.7652E-02	1.5940E-02	1.8362E 00	1.1013E-01	5.6649E 01	6.2727E 00
55	7.2008E 00	5.1852E 01	3.6518E-01	2.5357E-02	1.6489E-02	1.8025E 00	1.5319E-01	3.9437E 01	6.0648E 00

TABLE X
EXPERIMENTAL DATA FOR SAMPLE 4 AT ROTOR SPEED 13,410 RPM
(See Figure 7)

THE CONCENTRATION FOR THIS RUN = $0.1098E-00$
DIFFERENCE BTWN SQS OF BTM AND MENISCUS = $0.14738286E-02$
CONC. AT MENISCUS = $0.7052E-01$

Identification Number is Sample 4 13,410 RPM

I	R	X	CR	CX	C	LNC	CX/C	1/CX	1/C
1	6.1025E 00	3.7241E 01	1.0245E-02	8.3945E-04	7.0518E-02	-2.6519E 00	1.1904E-02	1.1913E 03	1.4181E 01
2	6.1261F 00	3.7529E 01	1.2984E-02	8.0598E-03	7.0792E-02	-2.6480E 00	1.4970E-02	1.7561E 02	1.4126E 01
3	6.1496F 00	3.7818E 01	1.5013E-02	1.2207E-03	7.1121E-02	-2.6434E 00	1.7163E-02	8.1923E 02	1.4000E 01
4	6.1732E 00	3.8128E 01	1.7245E-02	1.3968E-03	7.1501E-02	-2.6380E 00	1.9535E-02	7.1595E 02	1.3986E 01
5	6.1967E 00	3.8399E 01	1.9375E-02	1.5633E-03	7.1933E-02	-2.6320E 00	2.1733E-02	6.3966E 02	1.3902E 01
6	6.2213E 00	3.8692E 01	2.1607E-02	1.7368E-03	7.2451E-02	-2.6253E 00	2.3984E-02	5.7577E 02	1.3890E 01
7	6.2438F 00	3.8985E 01	2.4379E-02	1.9171E-03	7.2952E-02	-2.6180E 00	2.6279E-02	5.2163E 02	1.3708E 01
8	6.2674E 00	3.9280E 01	2.6374E-02	2.1044E-03	7.3544E-02	-2.6099E 00	2.8610E-02	4.7526E 02	1.3597E 01
9	6.2919E 00	3.9576E 01	2.403E-02	2.2575E-03	7.4189E-02	-2.6011E 00	3.0428E-02	4.4297E 02	1.3479E 01
10	6.3145E 00	3.9873E 01	3.0838E-02	2.4418E-03	7.4887E-02	-2.5918E 00	4.2607E-02	4.0953E 02	1.3353E 01
11	6.3381E 00	4.0171E 01	3.3475E-02	2.6404E-03	7.5644E-02	-2.5817E 00	3.4911E-02	3.7867E 02	1.3220E 01
12	6.3616E 00	4.3470E 01	3.6911E-02	2.8303E-03	7.6463E-02	-2.5710E 00	3.7016E-02	3.5331E 02	1.3078E 01
13	6.3852E 00	4.3770E 01	3.8547E-02	3.0185E-03	7.7334E-02	-2.5595E 00	3.9028E-02	3.3129E 02	1.2930E 01
14	6.4087F 00	4.172E 01	4.0880E-02	4.1894E-03	7.8176E-02	-2.5475E 00	4.0746E-02	3.1354E 02	1.2775E 01
15	6.4323E 00	4.1374E 01	4.3721E-02	3.3985E-03	7.9273E-02	-2.5349E 00	4.2871E-02	2.9424E 02	1.2615E 01
16	6.4559E 00	4.1678E 01	4.6662E-02	3.6140E-03	8.0337E-02	-2.5215E 00	4.4985E-02	2.7670E 02	1.2448E 01
17	6.4794E 00	4.1983E 01	4.9198E-02	3.7965E-03	8.1466E-02	-2.5076E 00	4.6603E-02	2.6603E 02	1.2225E 01
18	6.5030E 00	4.2248E 01	4.0168E-03	8.2661E-03	8.2493E-02	-2.4930E 00	4.8593E-02	2.4896E 02	1.2098E 01
19	6.5265E 00	4.2595E 01	5.5589E-02	4.2587E-03	8.3931E-02	-2.4778E 00	5.0741E-02	2.3481E 02	1.1915E 01
20	6.5501E 00	4.2903E 01	5.8835E-02	4.4912E-03	8.5278E-02	-2.4618E 00	5.2665E-02	2.2266E 02	1.1726E 01
21	6.5736E 00	4.3212E 01	6.1980E-02	4.7143E-03	8.6701E-02	-2.4453E 00	5.4374E-02	2.1127E 02	1.1544E 01
22	6.5972E 00	4.5429E-01	6.5423E 01	4.9588E-03	8.8202E-02	-2.4281E 00	5.6222E-02	2.0166E 02	1.1338E 01
23	6.6207E 00	4.3834E 01	6.9182E-02	5.2247E-03	8.9787E-02	-2.4103E 00	5.8189E-02	1.9140E 02	1.1137E 01
24	6.6443F 00	4.4147E 01	7.3240E-02	5.5115E-03	9.1465E-02	-2.3918E 00	6.0258E-02	1.8144E 02	1.0933E 01
25	6.6679E 00	4.4466E 01	7.7602E-02	5.8191E-03	9.3241E-02	-2.3726E 00	6.2409E-02	1.7187E 02	1.0725E 01
26	6.6914E 00	4.4775E 01	8.2166E-02	6.1397E-03	9.5123E-02	-2.3526E 00	6.4545E-02	1.6287E 02	1.0513E 01
27	6.7150E 00	4.5091E 01	8.7238E-02	6.4958E-03	9.7118E-02	-2.3318E 00	6.6886E-02	1.5394E 02	1.0291E 01
28	6.7385E 00	4.5408E 01	9.2412E-02	6.9570E-03	9.9234E-02	-2.3103E 00	6.9099E-02	1.4584E 02	1.0077E 01
29	6.7621E 00	4.5726E 01	9.8379E-02	7.2755E-03	1.0148E-01	-2.2879E 00	7.1695E-02	1.3744E 02	9.8541E 00
30	6.7856E 00	4.6045E 01	1.0479E-01	7.7213E-03	1.0387E-01	-2.2646E 00	7.4333E-02	1.2956E 02	9.6277E 00
31	6.8092E 00	4.6365E 01	1.1158E-01	8.1936E-03	1.0642E-01	-2.2403E 00	7.6992E-02	1.2205E 02	9.3955E 00
32	6.8327E 00	4.6686E 01	1.1970E-01	8.7592E-03	1.0915E-01	-2.2151E 00	8.0252E-02	1.1417E 02	9.1626E 00
33	6.8563E 00	4.7008E 01	1.2610E-01	9.2610E-03	1.1207E-01	-2.1887E 00	8.3308E-02	1.0712E 02	8.9235E 00
34	6.8798E 00	4.7323E 01	1.3776E-01	1.0012E-02	1.1519E-01	-2.1611E 00	8.6910E-02	9.9885E 01	8.6810E 00
35	6.9034E 00	4.7657E 01	1.4810E-01	1.0727E-02	1.1856E-01	-2.1323E 00	9.0475E-02	9.3225E 01	8.4345E 00
36	6.9270E 00	4.7983E 01	1.5957E-01	1.1518E-02	1.2218E-01	-2.1022E 00	9.4265E-02	8.6823E 01	8.1844E 00
37	6.9505E 00	4.8310E 01	1.7296E-01	1.2442E-02	1.2610E-01	-2.0707E 00	9.8667E-02	8.0374E 01	7.9302E 00
38	6.9741E 00	4.8638E 01	1.8844E-01	1.3513E-02	1.3036E-01	-2.0375E 00	1.03666E-01	7.4005E 01	7.6713E 00
39	6.9976E 00	4.8967E 01	2.0846E-01	1.4489E-02	1.3503E-01	-2.0022E 00	1.1031E-01	6.7137E 01	7.4057E 00
40	7.0212E 00	4.9297E 01	2.3433E-01	1.6687E-02	1.4025E-01	-1.9644E 00	1.1898E-01	5.9927E 01	7.1303E 00
41	7.0447E 00	4.9628E 01	2.8910E-01	2.0519E-02	1.4641E-01	-1.9213E 00	1.4015E-01	4.8735E 01	6.8301E 00
42	7.0683E 00	4.9961F 01	3.3780E-01	2.3895E-02	1.5379E-01	-1.8722E 00	1.5537E-01	4.1850E 01	6.5023E 00
43	7.0919E 00	5.0294E 01	4.2909E-01	3.0252E-02	1.6282E-01	1.8151E 00	1.8580E-01	3.3055E 01	6.1466E 00
44	7.1154E 00	5.0629E 01	5.2749E-01	3.7067E-02	1.7409E-01	-1.7482E 00	2.6929E-01	5.7442E 01	5.7442E 00
45	7.1396E 00	5.0955E 01	6.8942E-01	4.8912E-02	1.8842E-01	-1.6691E 00	2.5640E-01	5.3072E 01	5.0726E 00
46	7.1625E 00	5.1302E 01	1.0651E 00	5.0908E-02	2.0908E-01	-1.5650E 00	3.5562E-01	4.7828E 00	4.3496E 00
47	7.1961F 00	5.1640E 01	1.2747E 00	1.3410E-01	2.4431E-01	-1.4939E 00	5.4890E-01	4.0931E 00	4.0931E 00
48	7.2096E 00	5.1979E 01	2.7490E 00	1.9065E-01	2.9938E-01	-1.2061E 00	6.3688E-01	3.3403E 00	3.3403E 00

TABLE XI
EXPERIMENTAL DATA FOR SAMPLE 4 AT ROTOR SPEED 10,659 RPM
(See Figure 8)

THE CONCENTRATION FOR THIS RUN = 0.1098E-00
DIFFERENCE B/TWN SQS OF BTM AND MENISCUS = 0.14800723E-02
CONC. AT MENISCUS = 0.7316E-01

I	R	X	CR	CX	C	LN(C)	CX/C	1/CX	1/C
1	6.1057E 00	3.7280E 01	2.4082E-02	1.9721E-03	7.3156E-02	-2.6152E 00	2.6957E-02	5.0708E 02	1.3669E 01
2	6.1349E 00	3.7637E 01	2.5742E-02	2.0980E-03	7.3884E-02	-2.6053E 00	2.8396E-02	4.7664E 02	1.3555E 01
3	6.1642E 00	3.7997E 01	2.7403E-02	2.598E-03	7.4661E-02	-2.5948E 00	4.4989E-02	4.4989E-02	1.3344E 01
4	6.1934E 00	3.8358E 01	3.0725E-02	2.4804E-03	7.5510E-02	-2.5835E 00	3.2849E-02	4.0315E 02	1.3232E 01
5	6.2226E 00	3.8721E 01	3.2386E-02	2.6022E-03	7.6433E-02	-2.5713E 00	3.4046E-02	3.8428E 02	1.3033E 01
6	6.2519E 00	3.9086E 01	3.4046E-02	2.7299E-03	7.7404E-02	-2.5587E 00	3.5178E-02	3.6726E 02	1.2919E 01
7	6.2811E 00	3.9452E 01	3.6538E-02	2.8436E-03	7.8436E-02	-2.5455E 00	3.7082E-02	3.4382E 02	1.2779E 01
8	6.3104E 00	3.9821E 01	3.9859E-02	3.1582E-03	7.9552E-02	-2.5313E 00	3.9700E-02	3.1663E 02	1.2570E 01
9	6.3396E 00	4.0190E 01	4.1520E-02	3.2747E-03	8.0742E-02	-2.5165E 00	4.0557E-02	3.0538E 02	1.2309E 01
10	6.3688E 00	4.0562E 01	4.2350E-02	3.3248E-03	8.1968E-02	-2.5014E 00	4.0562E-02	3.0077E 02	1.2200E 01
11	6.3981E 00	4.0935E 01	4.4011E-02	3.4394E-03	8.3230E-02	-2.4861E 00	4.1324E-02	2.9075E 02	1.2015E 01
12	6.4223E 00	4.1310E 01	4.6502E-02	3.6176E-03	8.4553E-02	-2.4704E 00	4.2784E-02	2.7643E 02	1.1827E 01
13	6.4555E 00	4.1687E 01	4.8994E-02	3.7941E-03	8.5949E-02	-2.4540E 00	4.4144E-02	2.6357E 02	1.1639E 01
14	6.4885E 00	4.2065E 01	5.0654E-02	3.9057E-03	8.7406E-02	-2.4372E 00	4.4677E-02	2.5608E 02	1.1441E 01
15	6.5115E 00	4.2445E 01	5.3146E-02	4.0787E-03	8.8923E-02	-2.4200E 00	4.5868E-02	2.4513E 02	1.1248E 01
16	6.5442E 00	4.2827E 01	5.6467E-02	4.3143E-03	9.0525E-02	-2.4021E 00	4.7658E-02	2.3179E 02	1.1047E 01
17	6.5735E 00	4.3211E 01	5.8128E-02	4.4214E-03	9.2200E-02	-2.3839E 00	4.7954E-02	2.2617E 02	1.0846E 01
18	6.6027E 00	4.3596E 01	5.9789E-02	4.5276E-03	9.3924E-02	-2.3653E 00	5.8205E-02	2.2087E 02	1.0647E 01
19	6.6319E 00	4.3983E 01	6.2280E-02	4.6955E-03	9.5708E-02	-2.3464E 00	4.9060E-02	2.1297E 02	1.0448E 01
20	6.6612E 00	4.4371E 01	6.4771E-02	4.8618E-03	9.7566E-02	-2.3272E 00	4.9831E-02	2.0568E 02	1.0250E 01
21	6.6904E 00	4.4762E 01	6.7262E-02	5.0268E-03	9.9496E-02	-2.3076E 00	5.0523E-02	1.9893E 02	1.0051E 01
22	6.7197E 00	4.5154E 01	6.8923E-02	5.125E-03	1.0149E-01	-2.4021E 00	5.1534E-02	1.9499E 02	9.8535E 00
23	6.7489E 00	4.5548E 01	7.3075E-02	5.4339E-03	1.0356E-01	-2.2676E 00	5.2277E-02	1.8471E 02	9.6561E 00
24	6.7781E 00	4.5943E 01	7.7227E-02	5.6968E-03	1.0576E-01	-2.2466E 00	5.3866E-02	1.7554E 02	9.4555E 00
25	6.8074E 00	4.6340E 01	8.3040E-02	6.0933E-03	1.0810E-01	-2.2247E 00	5.4622E-02	1.6395E 02	9.2506E 00
26	6.8366E 00	4.6739E 01	8.9633E-02	6.5590E-03	1.1063E-01	-2.2016E 00	5.5290E-02	1.5246E 02	9.0394E 00
27	6.8658E 00	4.7140E 01	9.7987E-02	7.1359E-03	1.1337E-01	-2.1771E 00	6.22943E-02	1.4014E 02	8.8207E 00
28	6.8951E 00	4.7542E 01	1.0878E-01	7.8884E-03	1.1639E-01	-2.1508E 00	6.7775E-02	1.2677E 02	8.5917E 00
29	6.9243E 00	4.7944E 01	1.2207E-01	8.8145E-03	1.1977E-01	-2.1222E 00	7.3598E-02	1.1345E 02	8.3496E 00
30	6.9535E 00	4.8352E 01	1.3702E-01	9.8522E-03	1.2355E-01	-2.0911E 00	7.9741E-02	1.0150E 02	8.0937E 00
31	6.9828E 00	4.8759E 01	1.5612E-01	1.1179E-02	1.2784E-01	-2.0570E 00	8.7444E-02	8.9457E 01	7.8225E 00
32	7.0120E 00	4.9168E 01	1.8186E-01	1.2968E-02	1.3278E-01	-2.0191E 00	9.7664E-02	7.7115E 01	7.5314E 00
33	7.0413E 00	4.9579E 01	2.1593E-01	1.5321E-02	1.3859E-01	-1.9762E 00	1.062E-01	6.5226E 01	7.2155E 00
34	7.0705E 00	4.9992E 01	2.7403E-01	1.9319E-02	1.4575E-01	-1.9259E 00	1.3296E-01	5.1603E 01	6.8610E 00
35	7.0991E 00	5.0406E 01	3.2801E-01	2.3100E-02	1.5455E-01	-1.8672E 00	1.4947E-01	4.3290E 01	6.4704E 00
36	7.1290E 00	5.0822E 01	4.3181E-01	3.0255E-02	1.6565E-01	-1.7979E 00	1.8282E-01	3.3019E 01	6.0367E 00
37	7.1582E 00	5.1240E 01	6.9754E-01	4.8123E-02	1.8215E-01	-1.7029E 00	2.6748E-01	5.4899E 01	5.4899E 00
38	7.1874E 00	5.1659E 01	1.1460E 00	7.9719E-02	2.0909E-01	-1.5650E 00	3.8127E-01	1.2544E 01	4.7827E 00
39	7.2167E 00	5.2080E 01	1.5030E 00	1.0414E-01	2.4780E-01	-1.3951E 00	4.2024E-01	9.6029E 00	4.0355E 00

TABLE XII
FINAL RESULTS OF THE ELEVEN EXPERIMENTS REPORTED

SAMPLE	ROTOR SPEED (RPM)	$M_1 \times 10^{-3}$	g_1	$-R_{11}$	$M_m \times 10^{-3}$	g_m	$-R_{mm}$	$+R_{1m}$
1	10,589	1.4	3.393×10^{-2}	6.16	28.9	2.135×10^{-7}	134	0.83
					50.2	1.715×10^{-10}	165	0.79
					97.7	9.757×10^{-17}	89	0.78
1	8,766	1.4	4.015×10^{-2}	6.24	30.1	1.022×10^{-5}	386	2.04
					38.6	8.520×10^{-6}	325	1.97
					67.4	1.427×10^{-6}	208	1.86
					82.6	4.047×10^{-7}	166	1.81
					105.5	5.114×10^{-8}	110	1.77
					112.9	2.545×10^{-8}	95	1.76
1	7,477	1.7	4.430×10^{-2}	5.90	29.6	1.413×10^{-4}	241	1.43
					59.3	1.301×10^{-5}	217	1.40
					131.3	6.394×10^{-8}	127	1.36
2	17,250	1.6	3.520×10^{-3}	20.0	5.2	8.288×10^{-5}	75	1.87
					43.8	1.187×10^{-20}	186	4.37
					116.3	6.127×10^{-48}	255	1.29
2	10,589	1.6	1.050×10^{-2}	20.0	44.5	1.381×10^{-7}	122	6.04
					58.6	1.222×10^{-8}	45	5.89
					62.1	6.474×10^{-9}	27	5.86
					66.6	2.874×10^{-9}	6	5.82
2	7,447	3.3	1.503×10^{-2}	13.2	32.7	5.616×10^{-5}	215	4.66
					114.3	2.545×10^{-8}	86	4.49
3	10,589	4.4	1.125×10^{-2}	5.3				
3	8,766	4.7	1.966×10^{-2}	4.7		No other significant components found for this fraction.		
3	7,447	4.2	2.740×10^{-2}	5.5				
4	13,410	1.6	1.901×10^{-2}	7.0	6.2	1.729×10^{-4}	164	2.11
					10.7	2.003×10^{-5}	160	2.12
					139.3	1.580×10^{-31}	117	2.32
4	10,589	1.6	2.422×10^{-2}	8.3	3.2	3.352×10^{-3}	136	6.02
					9.8	2.337×10^{-3}	38	0.92
					44.6	1.525×10^{-6}	373	3.85
					123.1	1.190×10^{-10}	1,558	5.41

The subscript m ($m = 2, 3, \dots$) indicates other fractions found.

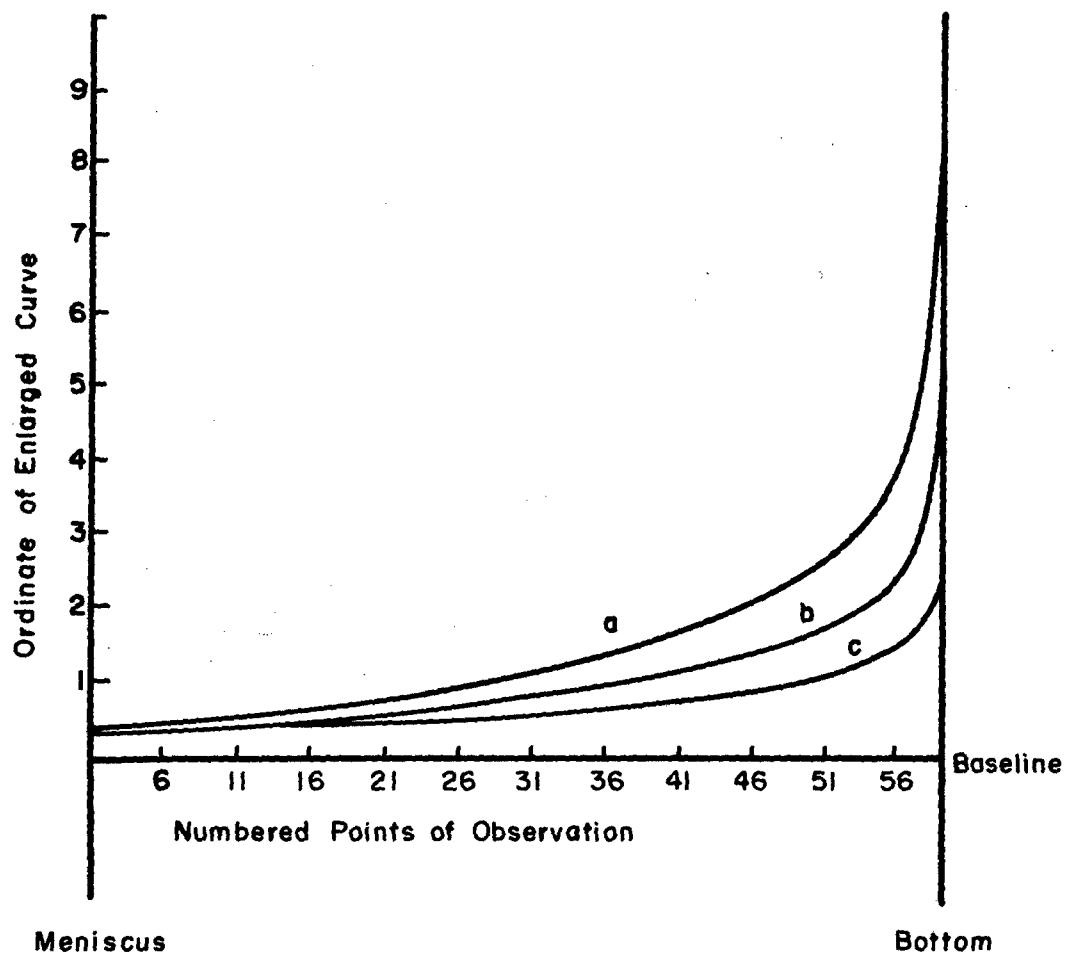


Figure 2. Schlieren Curves for Sample 1 at Rotor Speeds: a) 10,589 RPM; b) 8,766 RPM; and c) 7,447 RPM

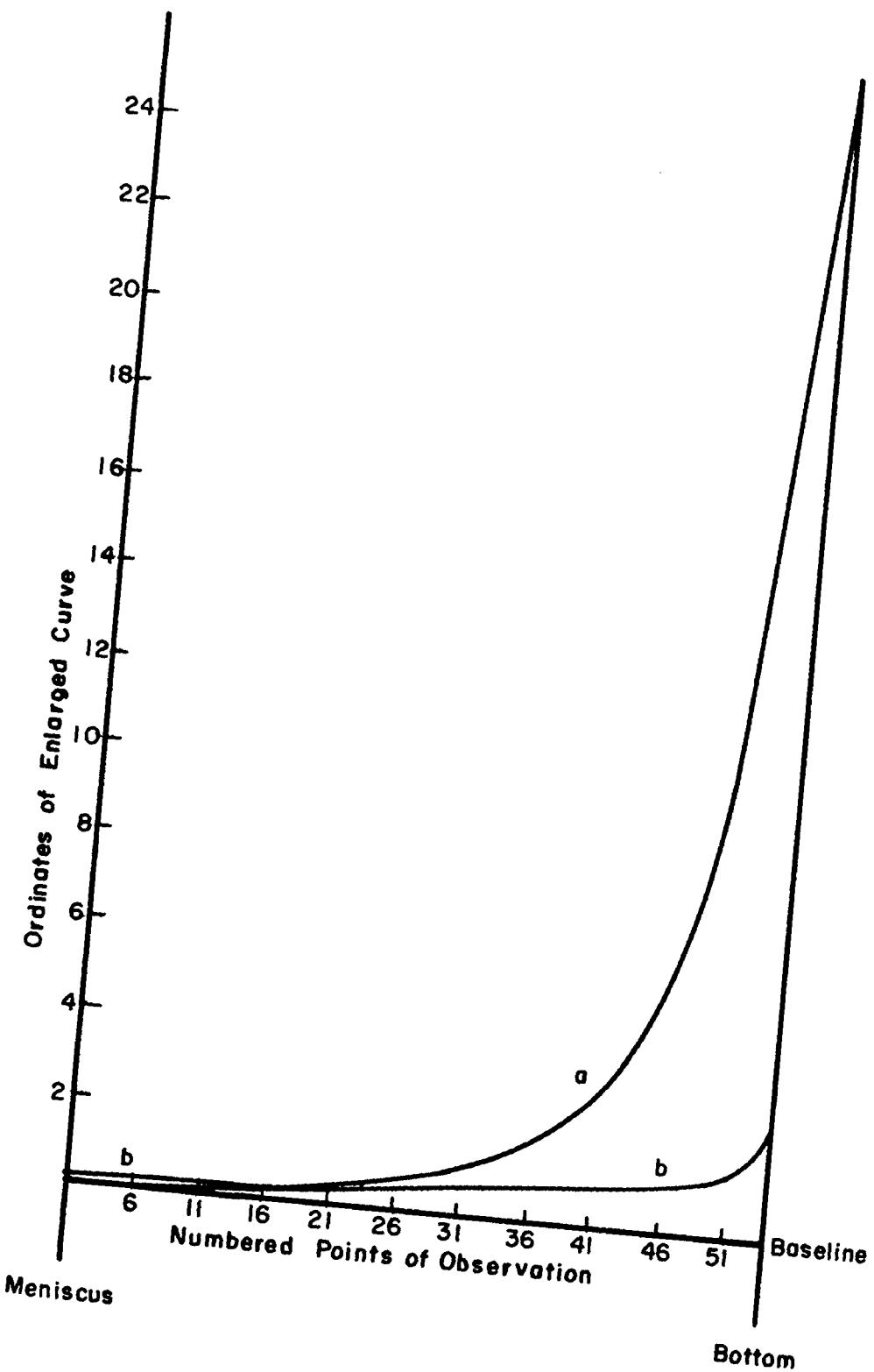


Figure 3. Schlieren Curve for Sample 2 at Rotor Speeds: a) 17,250 RPM; and
b) 7,447 RPM

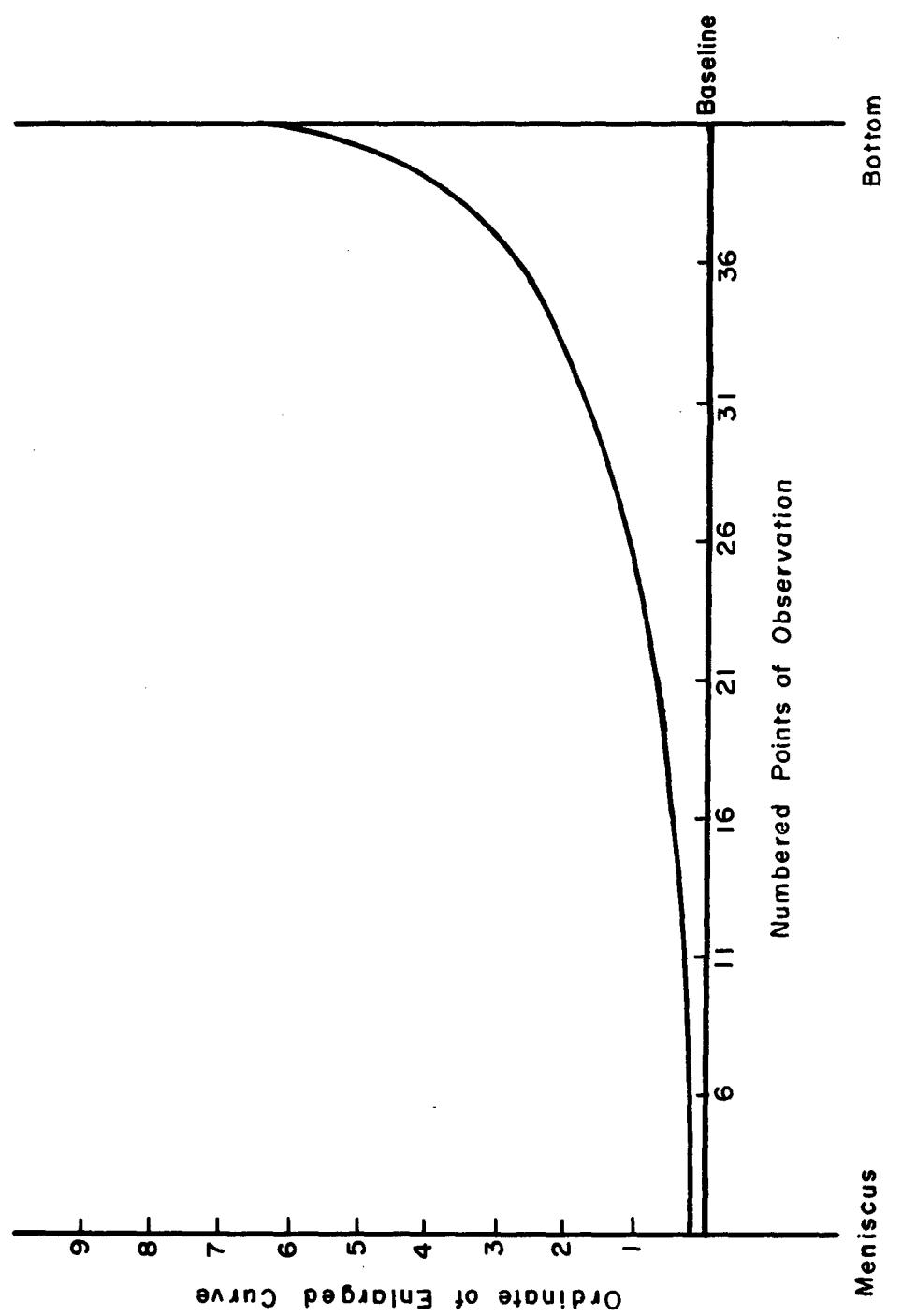


Figure 4. Schlieren Curve for Sample 2 at Rotor Speed 10,589 RPM

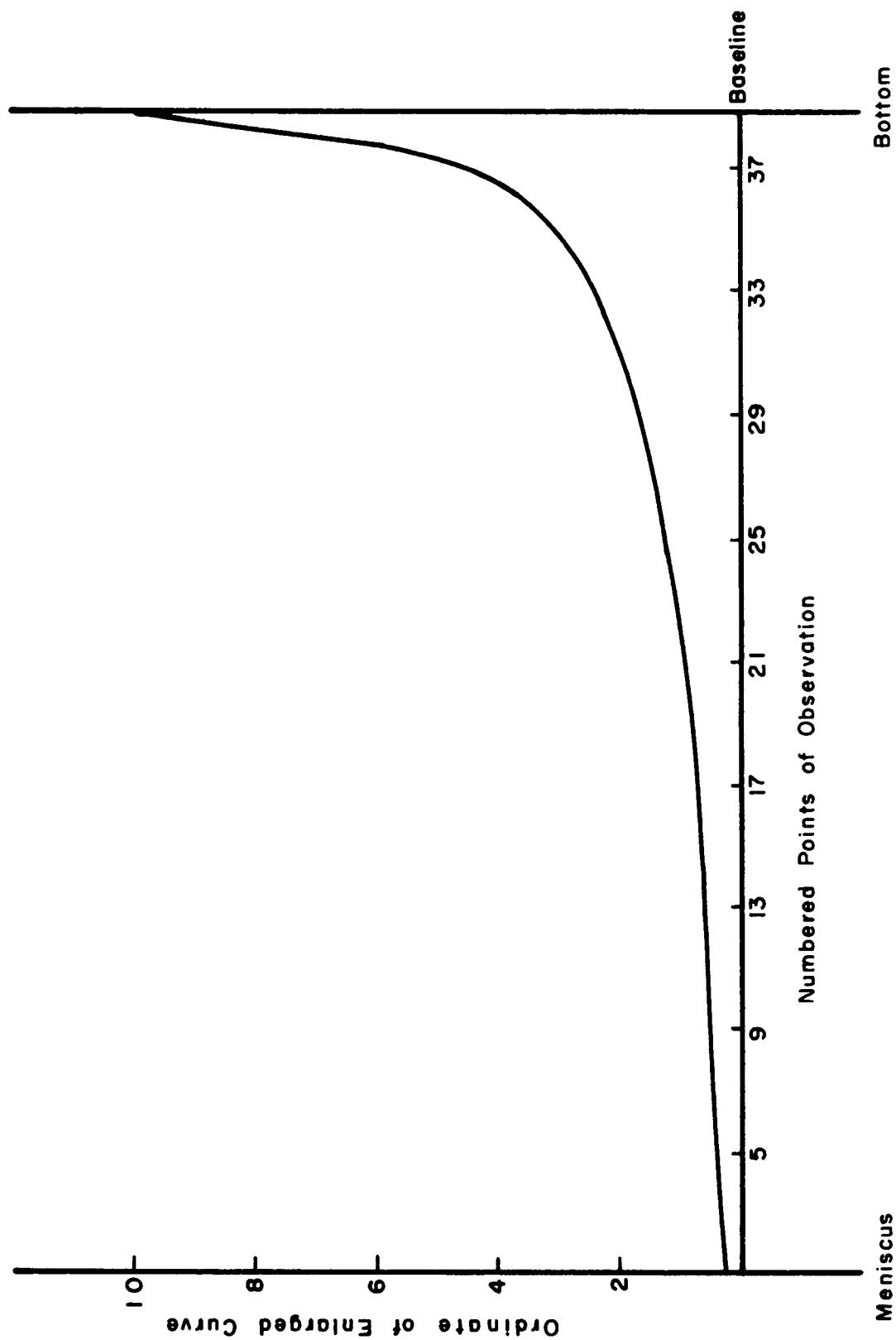


Figure 5. Schlieren Curve for Sample 3 at Rotor Speed 10,589 RPM

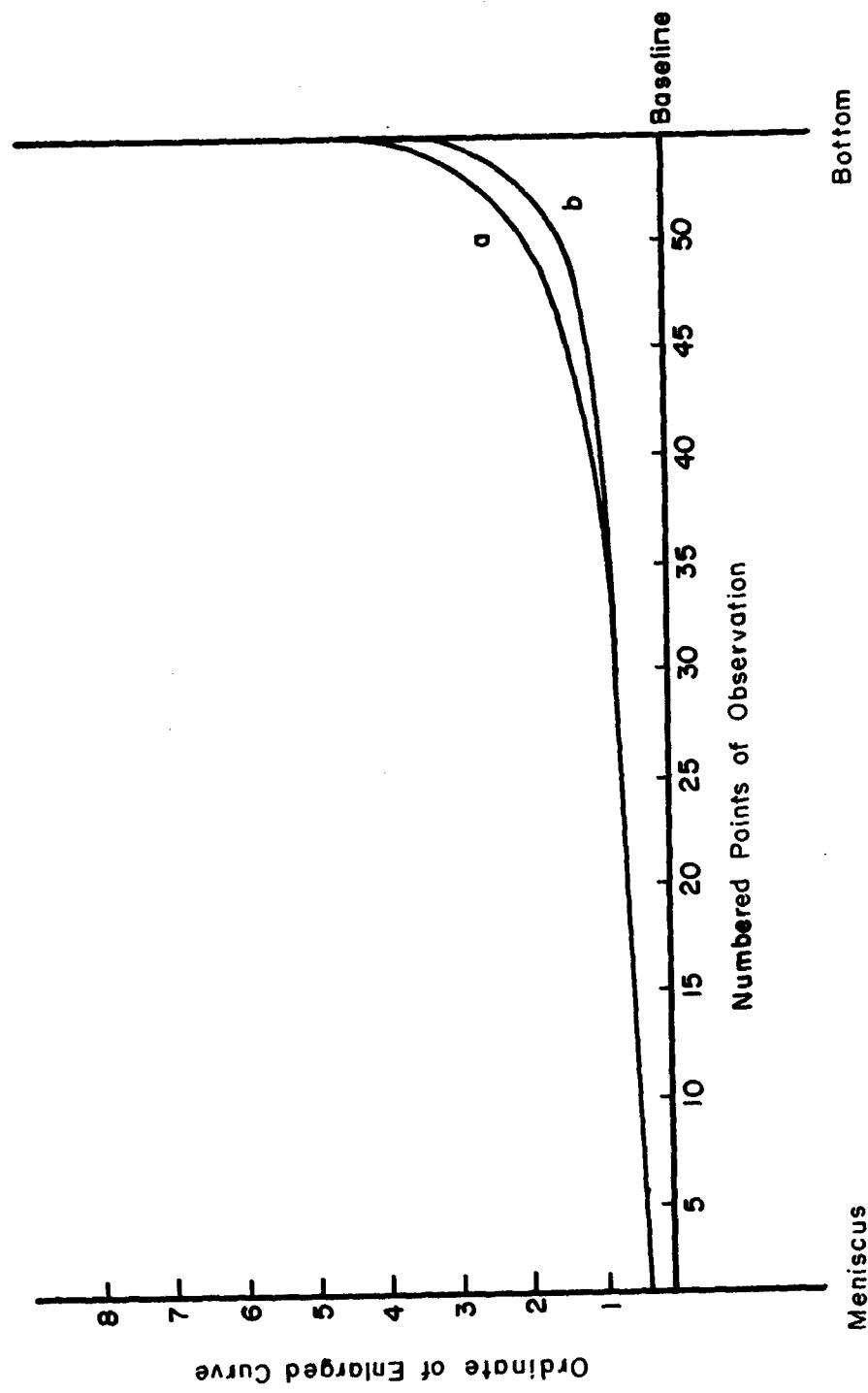


Figure 6. Schlieren Curve for Sample 3 at Rotor Speeds: a) 8,766 RPM; and
b) 7,447 RPM

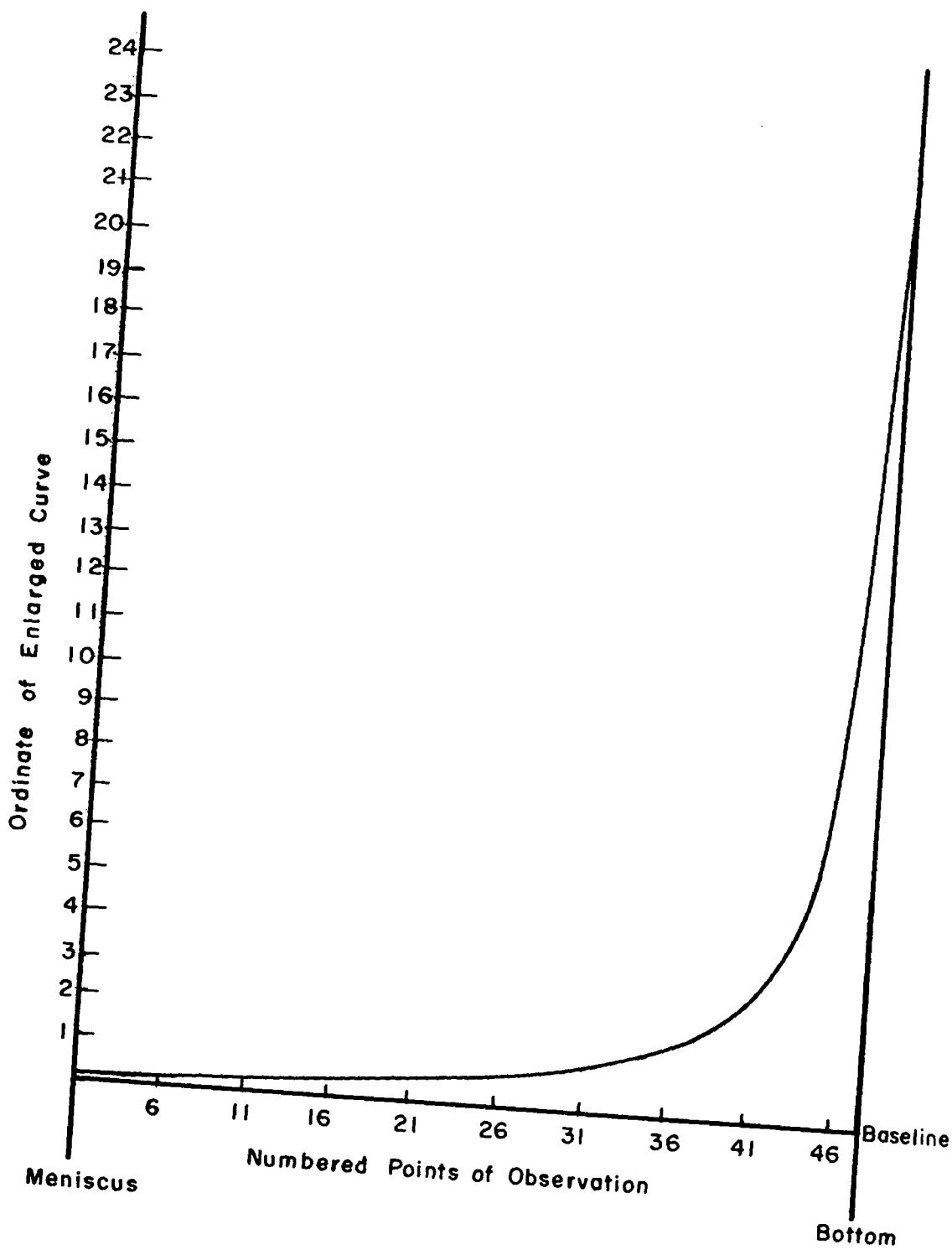


Figure 7. Schlieren Curve for Sample 4 at Rotor Speed 13,410 RPM

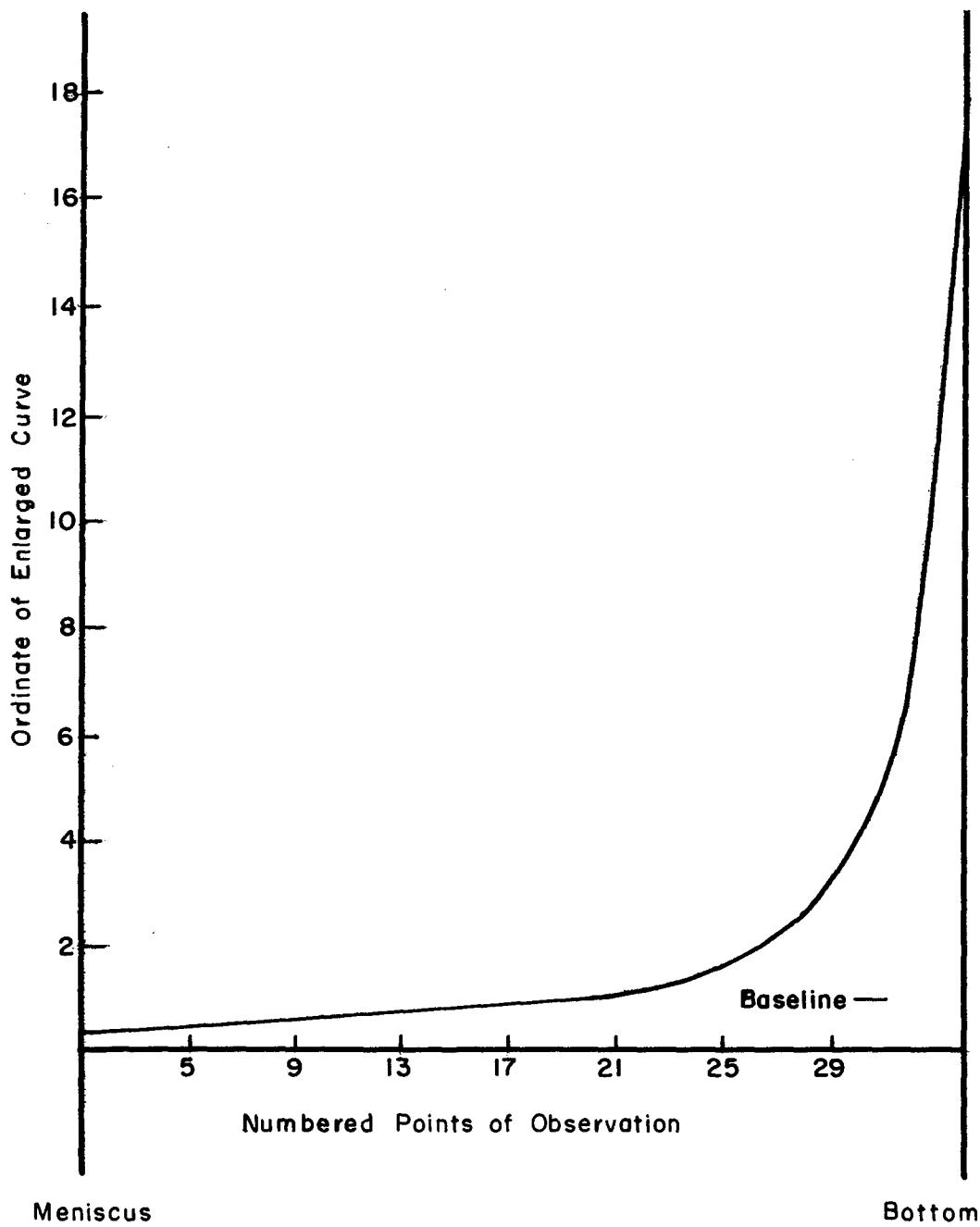


Figure 8. Schlieren Curve for Sample 4 at Rotor Speed 10,589 RPM

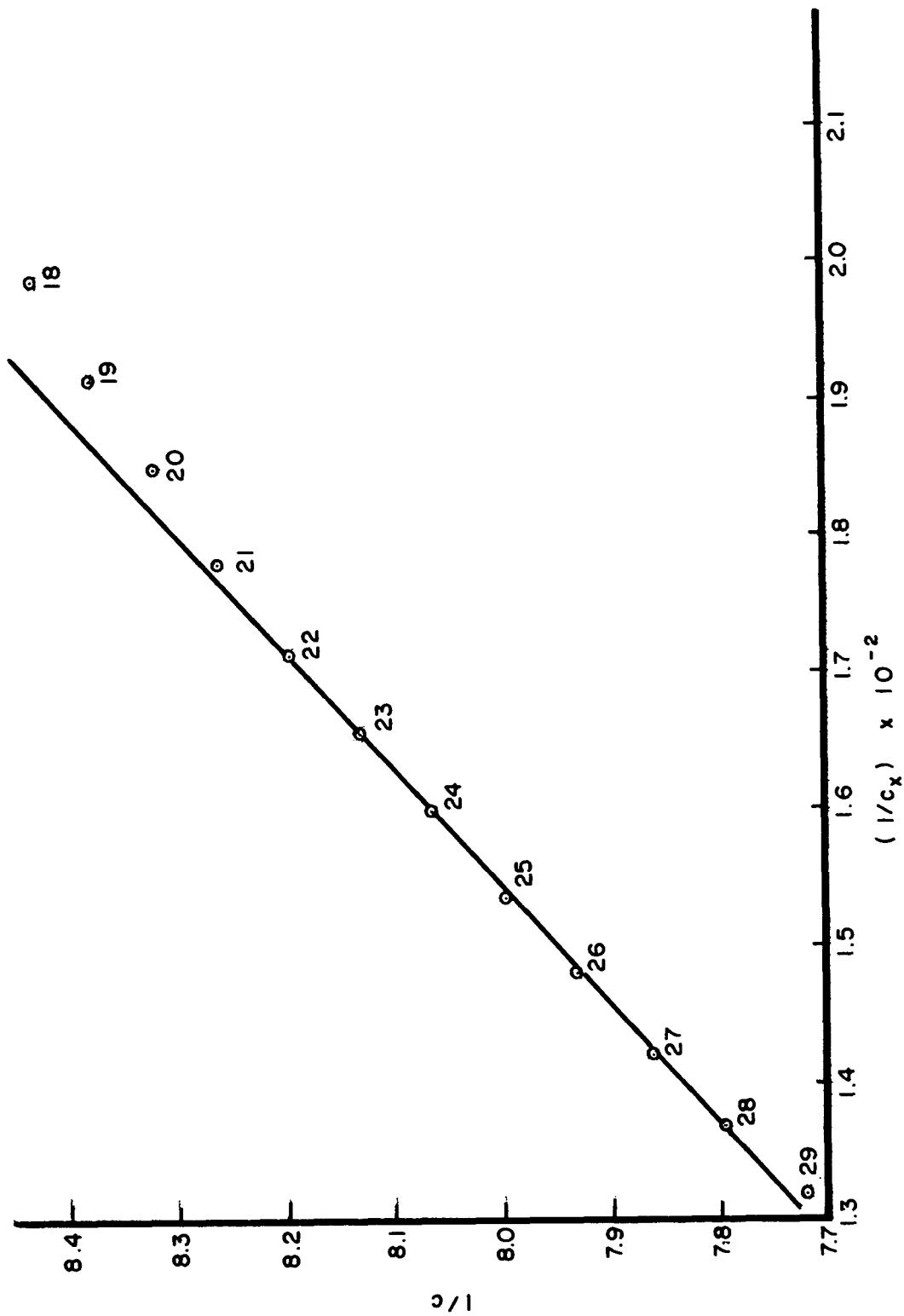


Figure 9. Equilibrium Sedimentation for Sample 1 at 10,589 RPM Showing Slope Equal to $h; \omega_2$

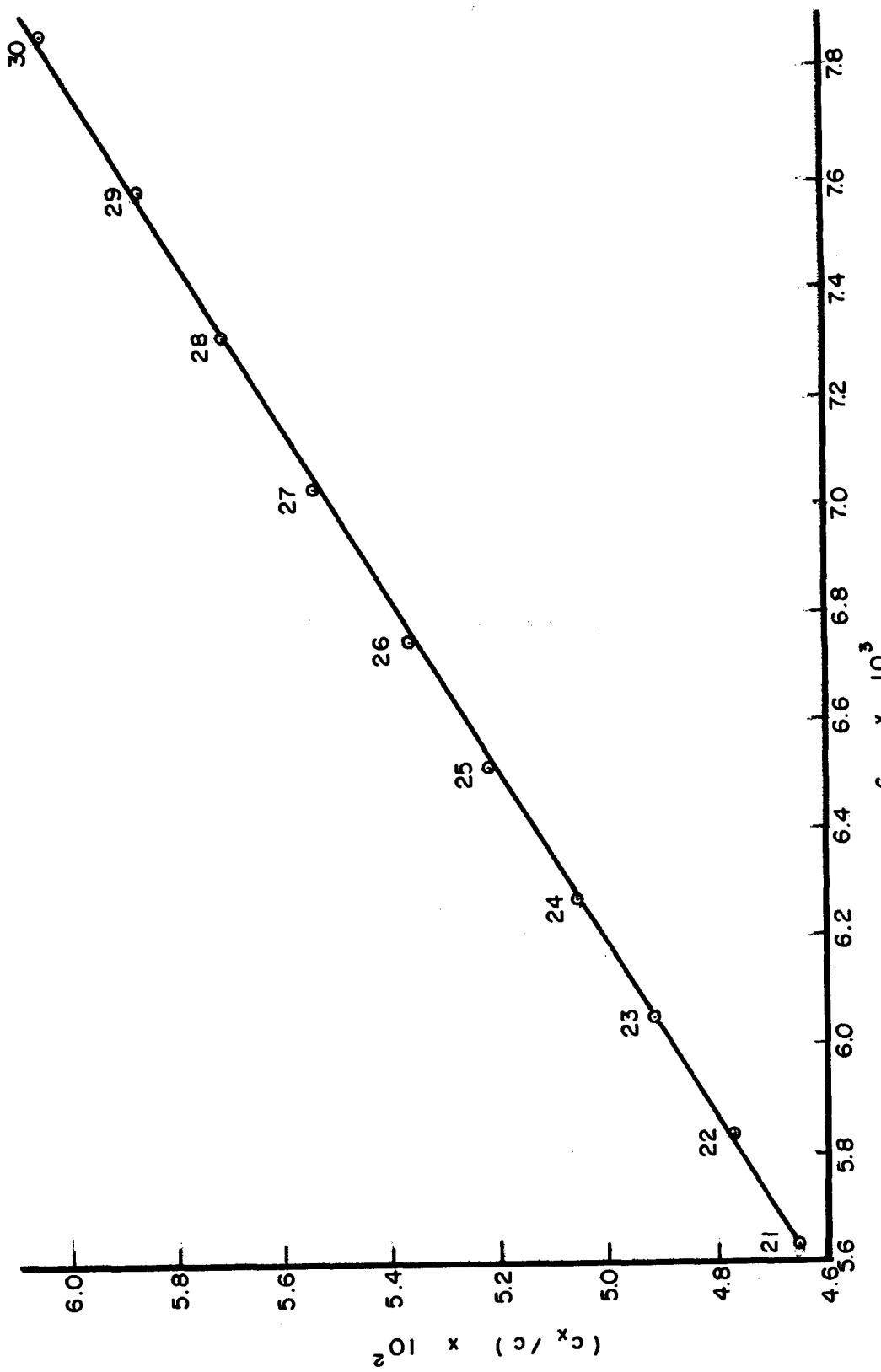


Figure 10. Equilibrium Sedimentation for Sample 1 at 10,589 RPM Showing Slope Equal to $-R_{1,1}$

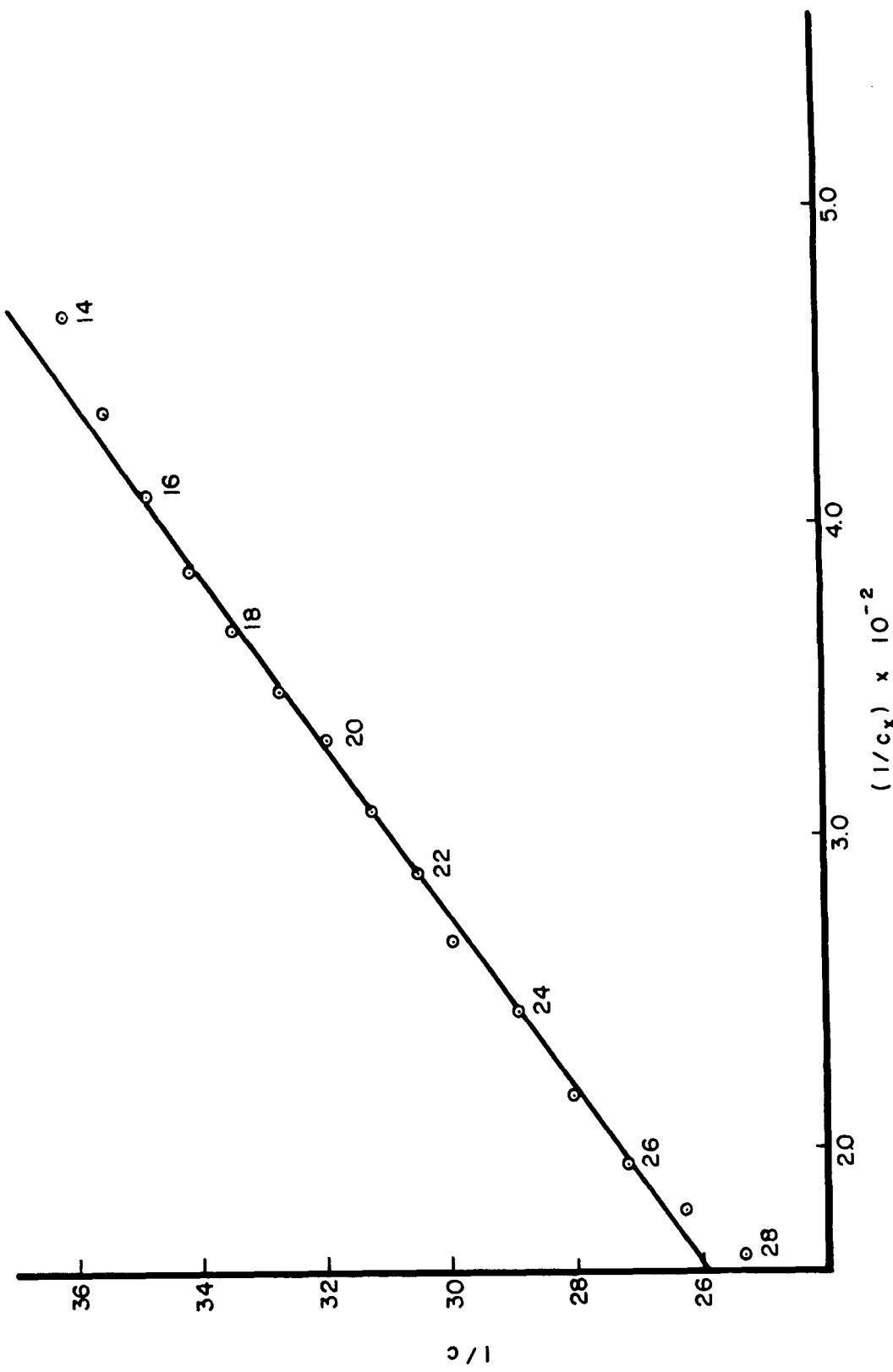


Figure 11. Equilibrium Sedimentation for Sample 2 at 17,250 RPM Showing Slope Equal to h, ω_2^2

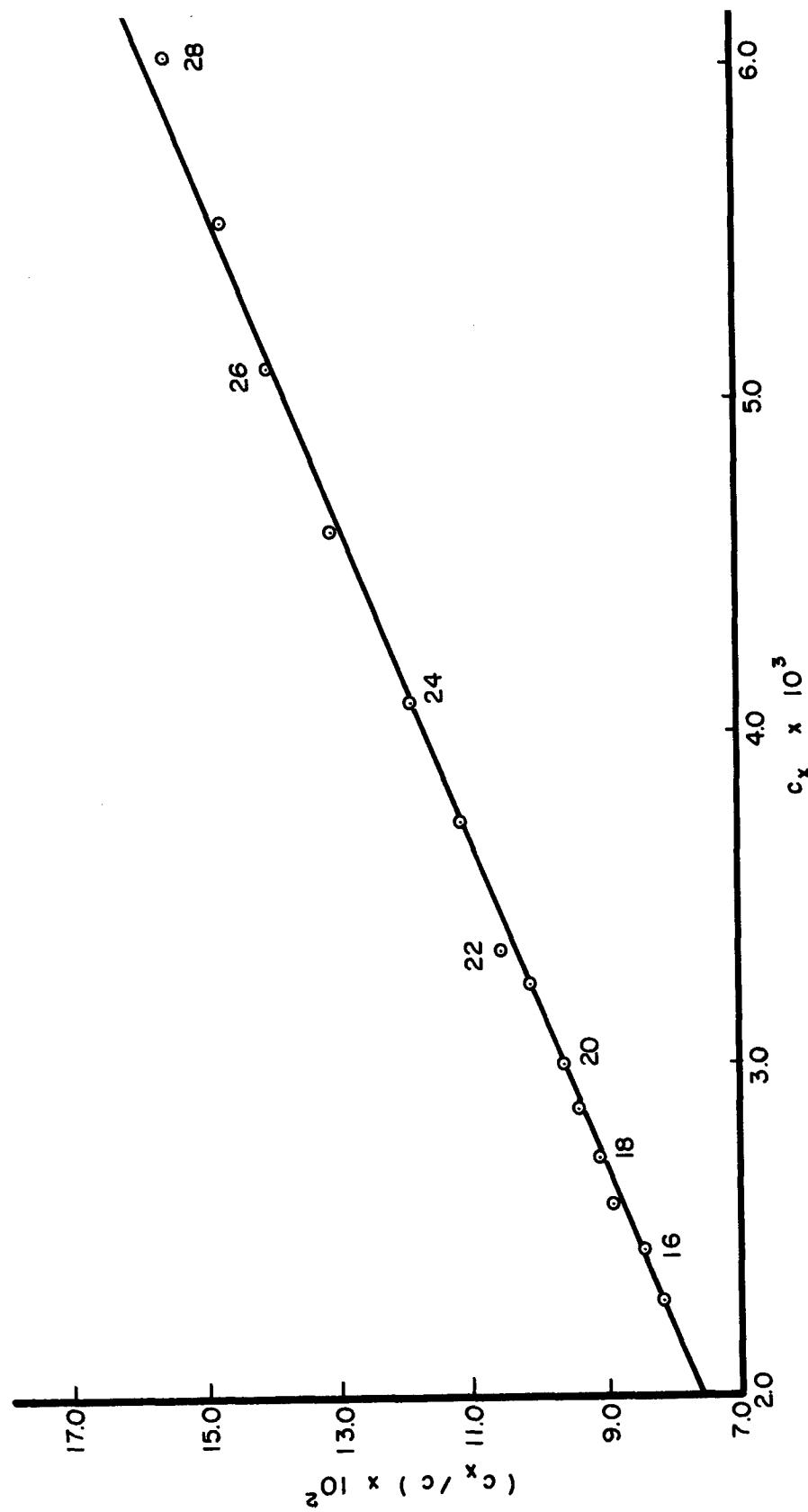


Figure 12. Equilibrium Sedimentation for Sample 2 at 17,250 RPM Showing
Equal to $-R_{1,1}$

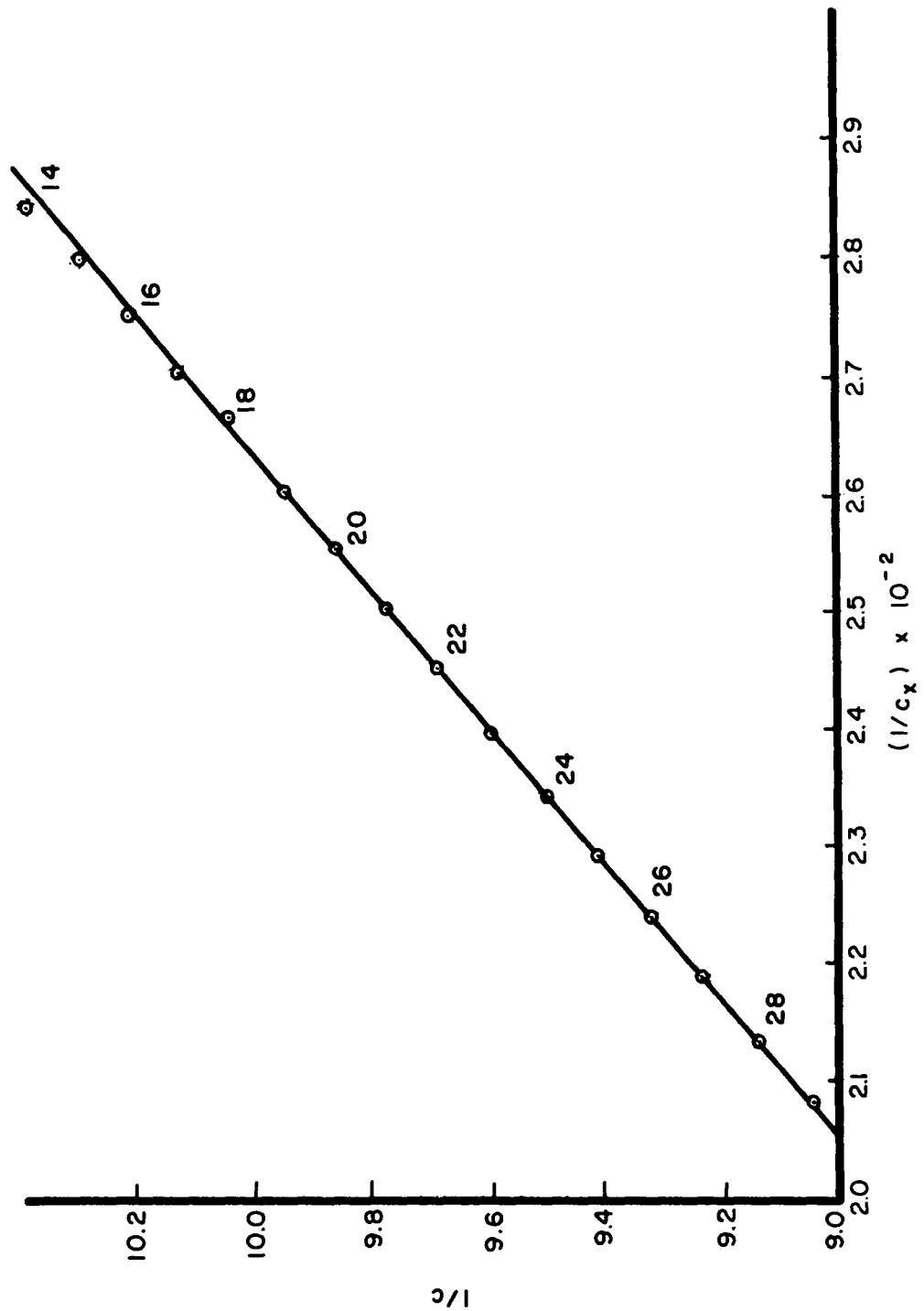


Figure 13. Equilibrium Sedimentation for Sample 3 at 7,447 RPM Showing Slope Equal to h, ω^2

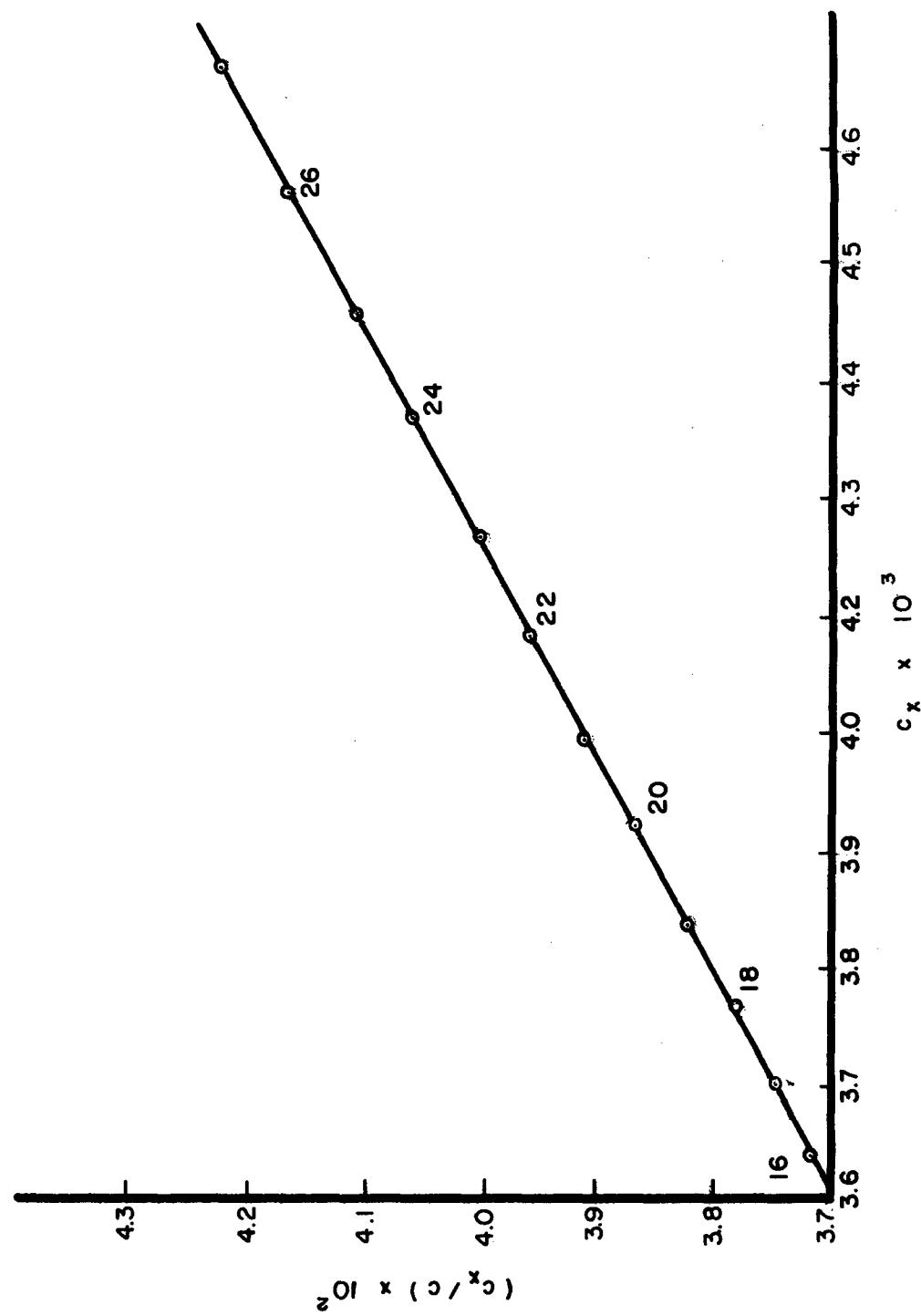


Figure 14* Equilibrium Sedimentation for Sample 3 at 7,447 RPM Showing
Slope Equal to $-R_{1,1}$

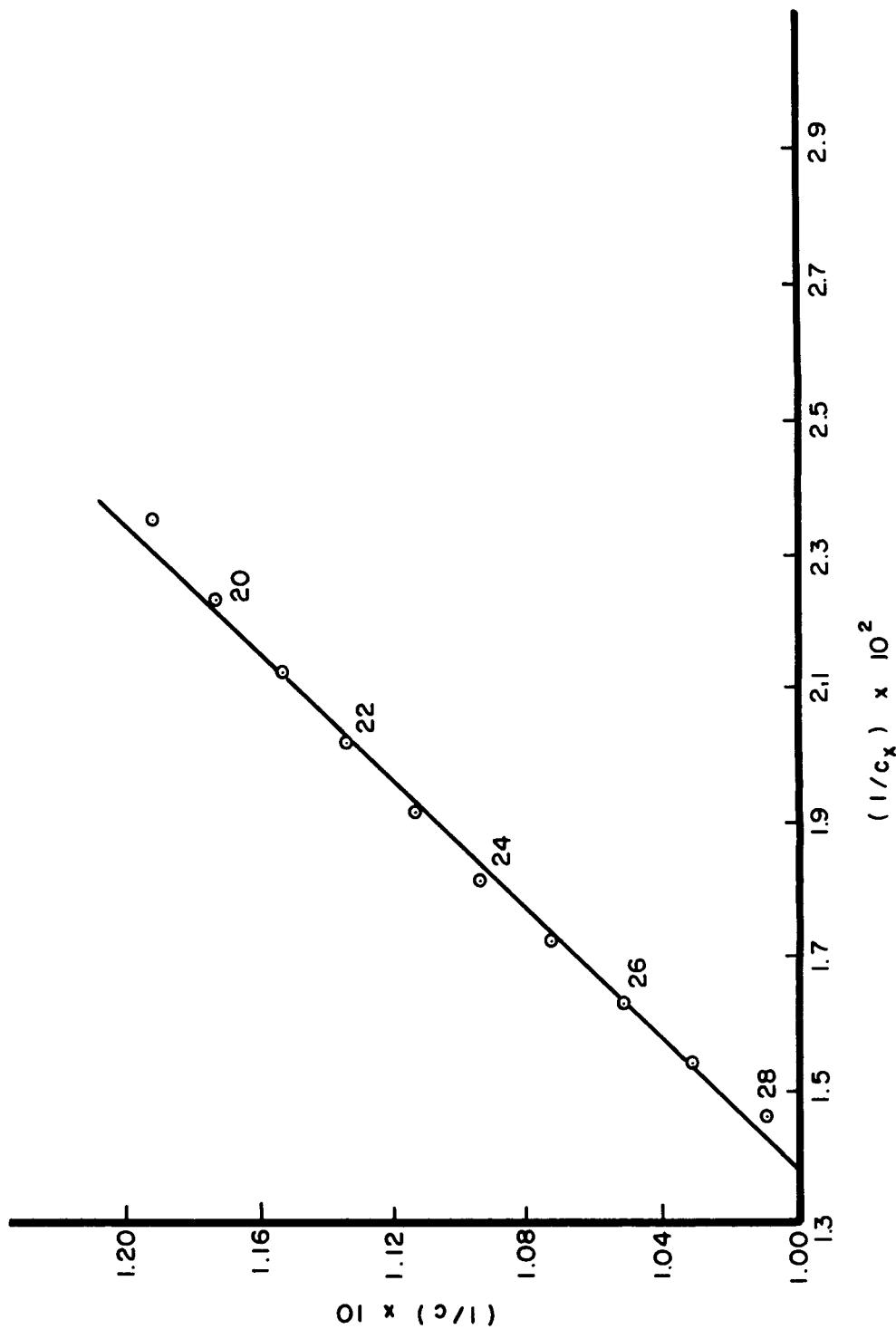


Figure 15. Equilibrium Sedimentation for Sample 4 at 13,410 RPM Showing
Slope Equal to h, ω_2

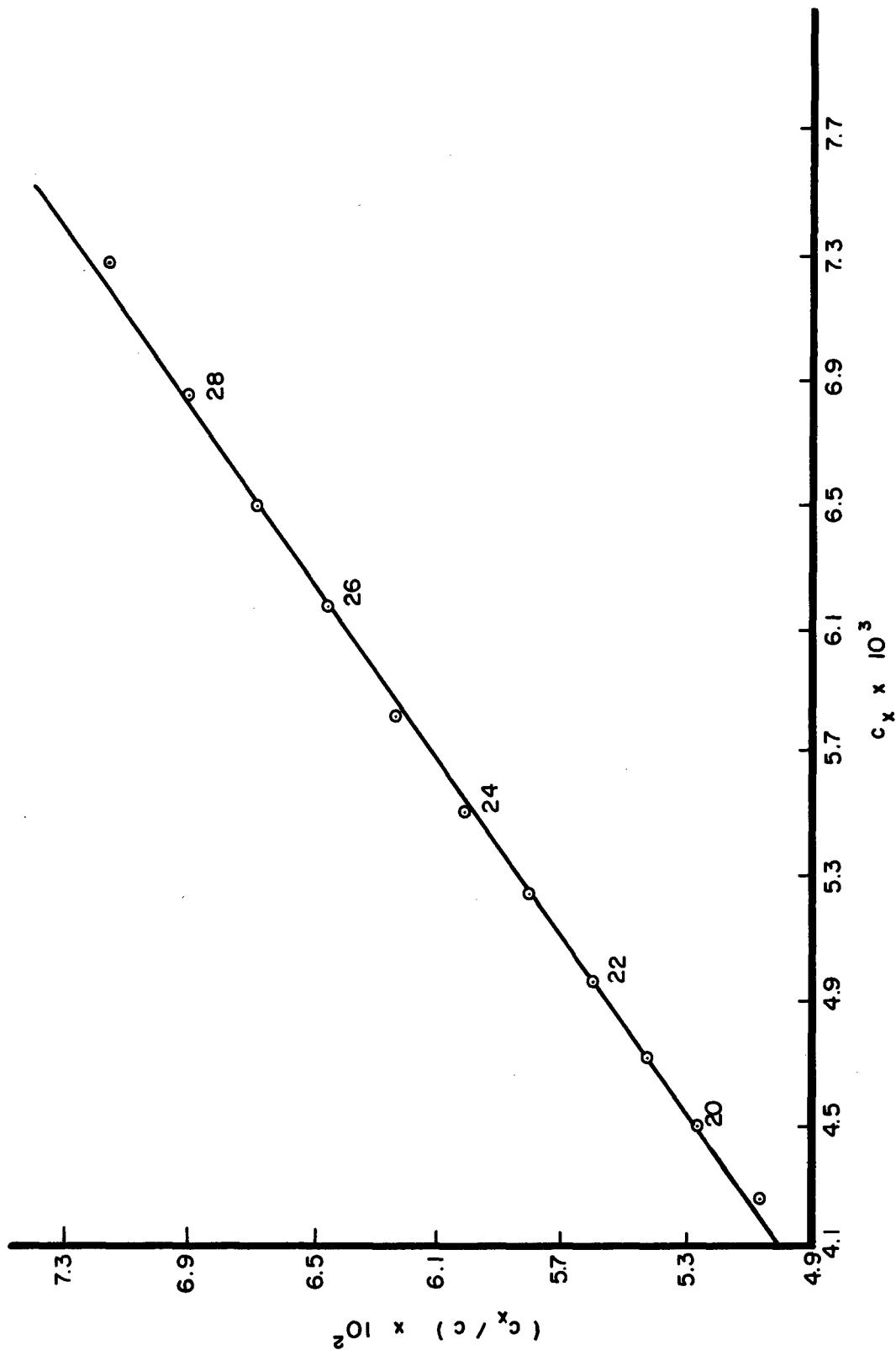


Figure 16. Equilibrium Sedimentation for Sample 4 at 13,410 RPM Showing Slope Equal to $-R_{1,1}$

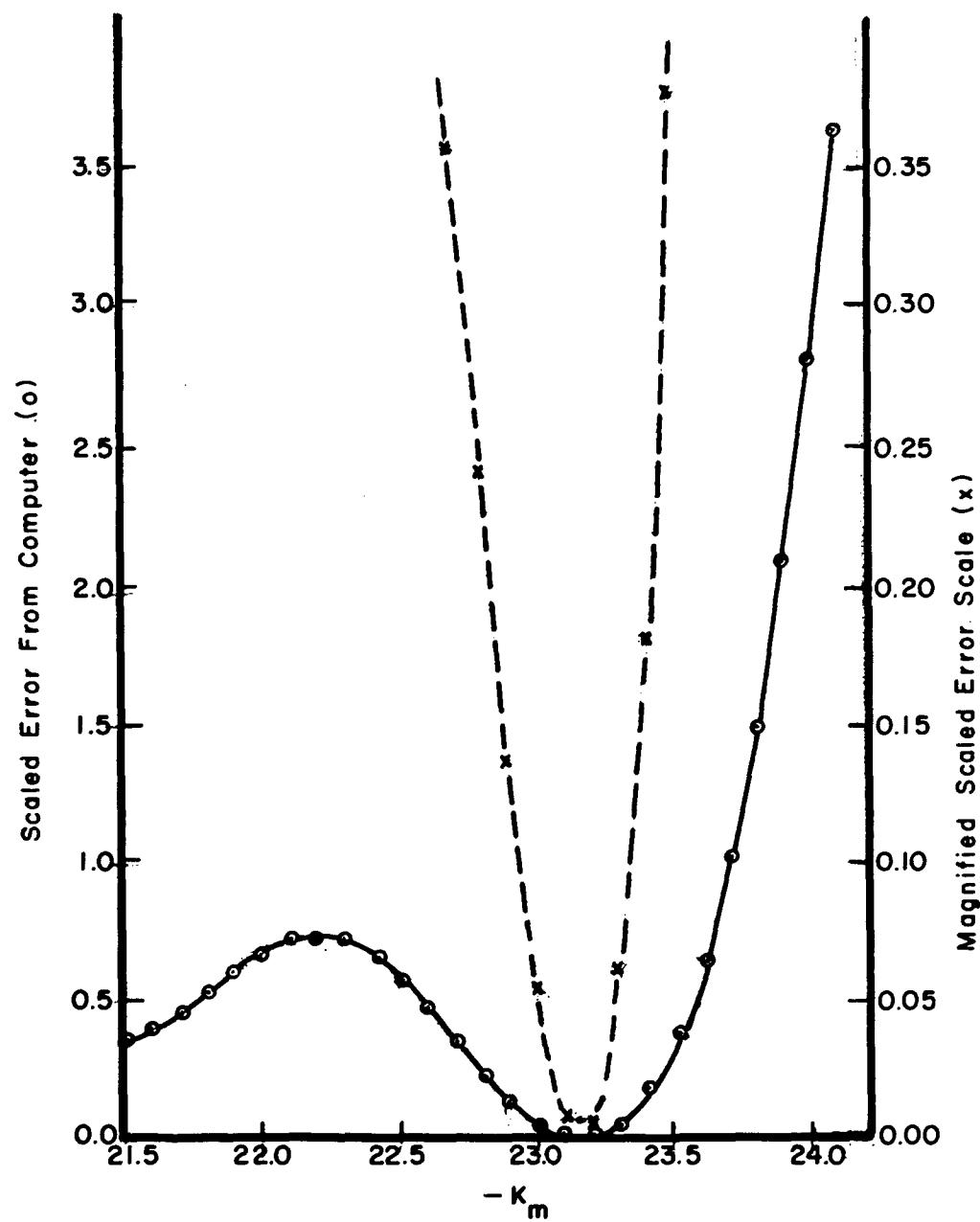


Figure 17. Error Δ_m^2 Vs. $(-K_m)$ for Sample 2 at 17,250 RPM, Indicating a Minimum at $K_m = 23.16$

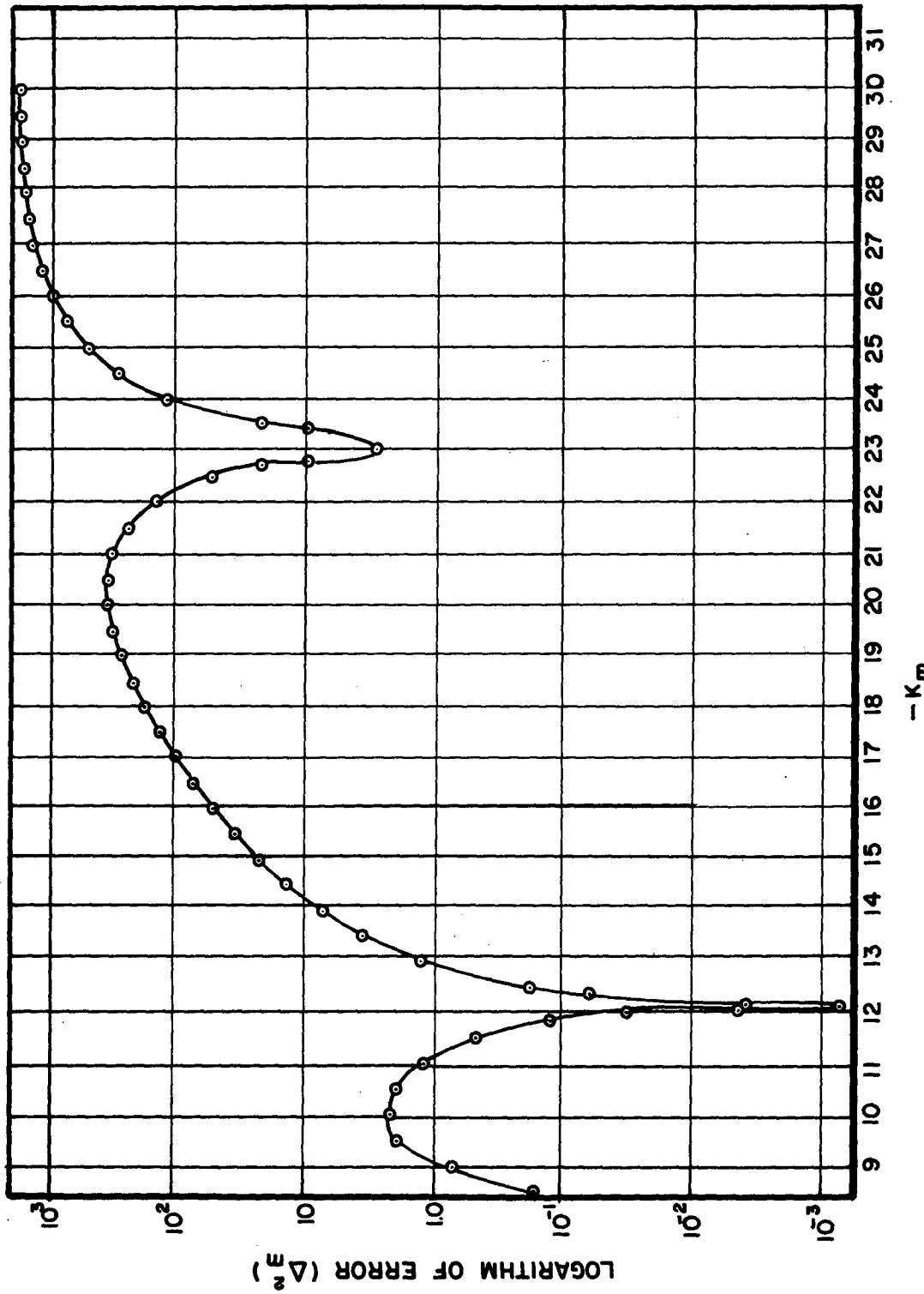


Figure 18. Example of How More Than One Fraction is Predicted (Each Minimum Corresponds to a Value K_m , and, Therefore, a Definite Fraction)

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13. ABSTRACT

Samples of dilute solutions of poly-2,2' (m-phenylene -5,5' bibenzimidazole) (PBI) in DMAC have been subjected to equilibrium sedimentation at 40°C. Each sample was composed of a very few distinct fractions, between 1 and 4. Since sedimentation of PBI in DMAC is characterized by strong concentration dependence, an appropriate computational method has been developed based on the formula:

$$c \approx \sum_{n=1}^N g_n \exp \left[h_n \omega^2 x - R_{nk} c + (R_{nk} - R_{nn}) c_n \right],$$

This method led to determination of molecular weights and other parameters characterizing fractions which appeared in each sample.

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